























		100 K	273 K	373 K	600 K	
	Air	=167.3	-13.5	3.4	19.0	
	An	-187.0	-21.7	-4.2	11.9	
	CH	107.0	-53.6	-21.2	81	
	CO <sub>3</sub>		-142	-72.2	-12.4	
	H.	-2.0	13.7	15.6		
	He	11.4	12.0	11.3	10.4	
	Kr		-62.9	-28.7	1.7	
	N <sub>2</sub>	-160.0	-10.5	6.2	21.7	
	Ne	-6.0	10.4	12.3	13.8	
		107.5	-22.0	-3.7	12.9	
	O <sub>2</sub>	-197.5				
Table 1	O <sub>2</sub> Xe Data: AIP, JI B' = B/KT. For Ar at 27:	-197.5 . The values relate to the expansic : K, $C = 1200 \text{ cm}^6 \text{ mol}^{-1}$ .	-153.7	-81.7	-19.6 ag	
Table 1.0	Q <sub>2</sub> Xe Data: AIP, II B' = B/RT. For Ar at 27:	- 197.3 . The values relate to the expansio 1 K, C = 1200 cm <sup>6</sup> mol <sup>-1</sup> .	-153.7 on in eqn 1.22 of Section 1.	-81.7 b; convert to eqn 1.21 usir	-19.6 ng -2)	b//10-2 day watch
Table 1.	O <sub>2</sub> Xe Data: AIP, II B <sup>-</sup> BIRT. For Ar at 27: 0 van der Waals coefficients a/(atm dm <sup>*</sup> mol <sup>-2</sup> )	- 197.5 The values relate to the expansio K, C = 1200 cm <sup>6</sup> mol <sup>-1</sup> . b/(10 <sup>-2</sup> dm <sup>3</sup> mol <sup>-1</sup> )	-153.7 on in eqn 1.22 of Section 1.	–81.7 b; convert to eqn 1.21 usir a/(atm dm <sup>6</sup> mol	-19.6 ag -2)	<i>b</i> /(10 <sup>-2</sup> dm <sup>3</sup> mol <sup>-1</sup> )
Table 1.	O <sub>2</sub> Xe Date: AIP, II B' = BIRT. For Ar at 27: 0 van der Waals coefficients a/(atm dm <sup>6</sup> mol <sup>-2</sup> ) 1.337	-197.5 The values relate to the expansion $K_{s} C = 1200 \text{ cm}^{6} \text{ mol}^{-1}$ . $b/(10^{-2} \text{ dm}^{3} \text{ mol}^{-1})$ 3.20	-153.7 on in eqn 1.22 of Section 1. H <sub>2</sub> S	-81.7 b; convert to eqn 1.21 usir <i>a</i> /(atm dm <sup>6</sup> mol 4.484	-19.6 ng -2)	b/(10 <sup>-2</sup> dm <sup>3</sup> mol <sup>-1</sup> ) 4.34
Table 1.	0,2 Xe 2,4 2,4 2,4 3,4 4,5 4,5 5,2 2,2 4,5 4,5 2,4 4,5 4,5 5,2 4,5 5,2 4,5 4,5 4,5 4,5 4,5 4,5 4,7 4,5 4,7 4,7 4,7 4,7 4,7 4,7 4,7 4,7	- 197.5 The values relate to the expansic K, C = 1200 cm <sup>4</sup> mol <sup>-1</sup> , b/(10 <sup>-3</sup> dm <sup>3</sup> mol <sup>-1</sup> ) 3.20 5.82	–153.7 on in eqn 1.22 of Section 1. H <sub>2</sub> S He	-81.7 b; convert to eqn 1.21 usir a/(atm dm <sup>6</sup> mol 4.484 0.0341	-19.6 <sup>19</sup> / <sub>9</sub> -2)	b/(10 <sup>-2</sup> dm <sup>3</sup> mol <sup>-1</sup> ) 4.34 2.38
Table 1.4 Ar C <sub>2</sub> H <sub>4</sub> C <sub>2</sub> H <sub>6</sub>	Q <sub>2</sub> Xe Date: AIP, II B <sup>+</sup> = NRT. For Ar at 27: 4 van der Waals coefficients <b>a</b> /(atm dm <sup>6</sup> mol <sup>-2</sup> ) 1.37 4.552 5.507	- 197.3 The values relate to the expansio K, C = 1200 cm <sup>6</sup> mol <sup>-1</sup> . b/(10 <sup>-2</sup> dm <sup>3</sup> mol <sup>-1</sup> ) 3.20 5.82 6.51	-153.7 on in eqn 1.22 of Section 1. H <sub>2</sub> S He Kr	-81.7 b; convert to eqn 1.21 usir a/(atm dm <sup>6</sup> mol 4.484 0.0341 5.125	-19.6 ag	b/(10 <sup>-2</sup> dm <sup>3</sup> mol <sup>-3</sup> ) 4.34 2.38 1.06
Table 1.0   Ar   C2H4   C2H6   C4H6	0,2 Xe Date: AIP, II B' = BIRT. For Ar at 27: 0 van der Waals coefficients a/(atm dm <sup>4</sup> mol <sup>-2</sup> ) 1.337 4.552 5.507 18.57	- 197.5 The values relate to the expansion K, <i>C</i> = 1200 cm <sup>6</sup> mol <sup>-1</sup> , <i>b</i> /(10 <sup>-2</sup> dm <sup>3</sup> mol <sup>-1</sup> ) 3.20 5.82 6.51 11.93 	-133.7 on in eqn 1.22 of Section 1. H <sub>2</sub> S He Kr N <sub>2</sub>	-81.7 bs convert to eqn 1.21 usir a/(atm dm <sup>6</sup> mol 4.484 0.0341 5.125 1.352	-19.6 ag	b/(10 <sup>-2</sup> dm <sup>3</sup> mol <sup>-3</sup> ) 4.34 2.38 1.06 3.87
Ar   C2H4   C2H6   C6H6   CH4	0,2 Xe 2,2 2,2 3 van der Waals coefficients a/(atm dm*mol <sup>-2</sup> ) 1.337 4.552 3.507 18.57 2.273 	-197.5 The values relate to the expansion $k_{\rm K} C = 1200  {\rm cm}^6  {\rm mol}^{-1}$ , $b/(10^{-2}  {\rm dm}^3  {\rm mol}^{-1})$ 3.20 5.82 6.51 11.93 4.31 	-153.7 on in eqn 1.22 of Section 1. H2S H2 Kr N3 N5 N5 N5	-81.7 ds convert to eqn 1.21 usin <i>al</i> /(atm dm <sup>4</sup> mol 4.484 0.3341 5.125 1.352 0.205 0.205	-19.6 ag -2)	b/(10 <sup>-2</sup> dm <sup>3</sup> mol <sup>-1</sup> ) 4.34 2.38 1.06 3.87 1.67
Ar   C2H4   C2H6   C6H6   CH4   C2	Q <sub>2</sub> Xe Date: AIP, II B' = NRT. For Ar at 27: 4 552 5.507 18.557 2.273 6.260 4.55 2	- 197.5 - The values relate to the expansio K, C = 1200 cm <sup>6</sup> mol <sup>-1</sup> .	-133.7 on in eqn 1.22 of Section 1. H <sub>2</sub> S H <sub>2</sub> S H <sub>6</sub> Kr Nf <sub>1</sub> Nf <sub>2</sub> Nf <sub>3</sub>	-81.7 ds convert to eqn 1.21 usir <i>a/(atm.dm<sup>4</sup> mol</i> 4.484 0.0341 5.125 1.352 0.205 4.109 1.24	-19.6 ag -2)	b/(10 <sup>-2</sup> dm <sup>3</sup> mol <sup>-1</sup> ) 4.34 2.38 1.06 3.87 1.67 3.71 2.10
Table 1.4   Ar   C <sub>2</sub> H <sub>4</sub> C <sub>2</sub> H <sub>6</sub> C <sub>6</sub> H <sub>6</sub> CH <sub>4</sub> Cl <sub>2</sub> CO	0,2 Xe Data: AIP, II B <sup>+</sup> = BRT. For Ar at 27: 0 van der Waals coefficients a/(atm dm <sup>4</sup> mol <sup>-2</sup> ) 1.337 4.552 5.507 18.57 2.273 6.260 1.453 2.610	-197.5 The values relate to the expansion $K_c C = 1200 \text{ cm}^6 \text{ mol}^{-1}$ . $b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$ 3.20 5.82 6.51 11.93 4.31 5.42 3.95 4.00	-133.7 on in eqn 1.22 of Section 1. H <sub>1</sub> S He Kr N <sub>5</sub> Ne NH <sub>3</sub> O <sub>7</sub> O <sub>7</sub>	-81.7 bs convert to eqn 1.21 usin a/(atm dm <sup>6</sup> mol 4.484 0.0341 5.125 1.352 0.205 4.169 1.364 6.775	-19.6 ag -2)	b/(10 <sup>-2</sup> dm <sup>3</sup> mol <sup>-3</sup> ) 4.34 2.38 1.66 3.87 1.67 3.71 3.19 5.ce
Table 1.   Ar   C2H4   C2H6   C8H6   CCH4   C12   CO   CO   H	0,2 Xe Date: AIP, II 0"= BIRT. For Ar at 27: 1.337 4.552 5.507 18.57 2.273 6.260 1.453 3.610 0.220	-197.5 The values relate to the expansion $k_{c} C = 1200 \text{ cm}^{6} \text{ mol}^{-1}$ . $b/(10^{-2} \text{ dm}^{3} \text{ mol}^{-1})$ 3.20 5.82 6.51 11.93 4.31 5.42 3.95 4.29 2.65	-153.7 on in eqn 1.22 of Section 1. H2S H2 Kr N5 N6 N6 N6 N6 N6 N6 N6 N6 N6 N6 N6 N6 N6	-81.7 ds convert to eqn 1.21 usin a/(atm dm <sup>6</sup> mol 4.484 0.0341 5.125 1.352 0.205 4.169 1.364 6.775 4.137	-19.6 ig	b/(10 <sup>-2</sup> dm <sup>3</sup> mol <sup>-1</sup> ) 4.54 2.38 1.06 3.87 1.67 3.71 3.71 3.19 5.68 5.16

