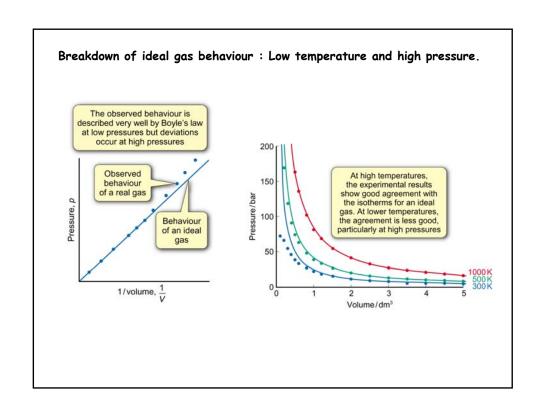
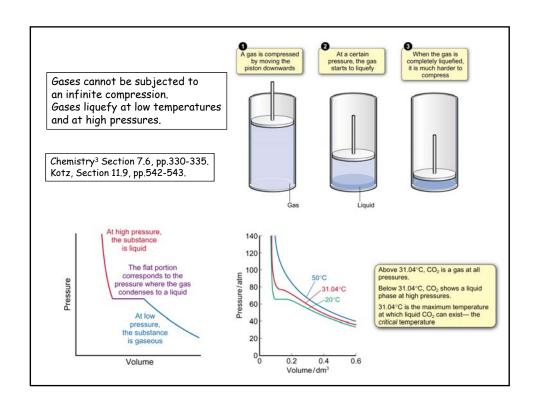
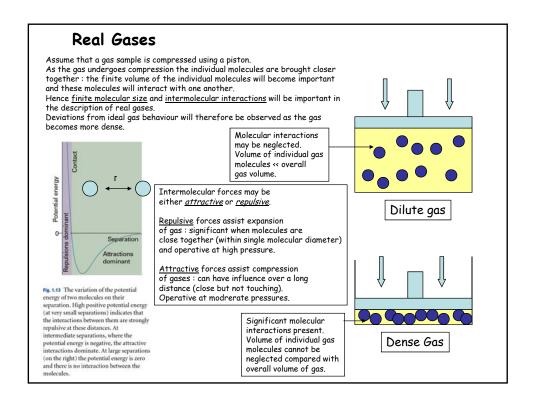


Ideal Gas behaviour: summary

- We recall the conditions under which the ideal gas equation of state PV=nRT is valid:
 - Volume of individual gas molecules is neglected
 - No interactions (either attractive or repulsive) exist amongst the molecules.
- These are not very reasonable assumptions. However the ideal gas approximation is useful for many gases at high temperatures or moderately low (< 10 atm) pressures, i.e. dilute gases.
- In the context of the kinetic molecular theory an ideal gas is one for which the mean free path λ (the distance over which the gas molecules travel before they experience collision) of the molecules is much greater than the collision diameter d.
- Also in an ideal gas the only contribution to the internal energy comes from the translational kinetic energy of the gas molecules. There is no contribution from the potential energy arising from interactions of gas molecules with each other.
- We now examine the behaviour of real gases.







Compressibility (Compression) Factor

We can express the extent of deviation from ideal behaviour as a function of pressure (which is related to the density of the gas) by introducing a quantity called the $\underline{\textit{Compressibility}}$ or $\underline{\textit{Compression factor}}$ Z.

$$Z = \frac{PV}{nRT} = \frac{PV_m}{RT}$$

Foe an ideal gas Z = 1, and real gases exhibit Z values different from unity. Z values may be explained in terms of the operation of <u>intermolecular forces</u>.

At low pressures the molecules are far apart and the predominant intermolecular interaction is <u>attraction</u>. The molar volume V_{m} is less than that expected for an ideal gas: intermolecular forces tend to draw the molecules together and so reduce the space which they occupy. Under such conditions we expect that $Z \!<\! 1$.

As the pressure is increased the average distance of separation between molecules decreases and $\frac{\text{repulsive}}{\text{pressure}} \text{ interactions between molecules become more important. Under such conditions we expect that Z > 1. When Z > 1, the molar volume is greater than that exhibited by an ideal gas: repulsive forces tend to drive the molecules apart.$

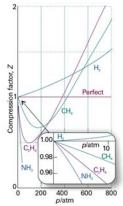
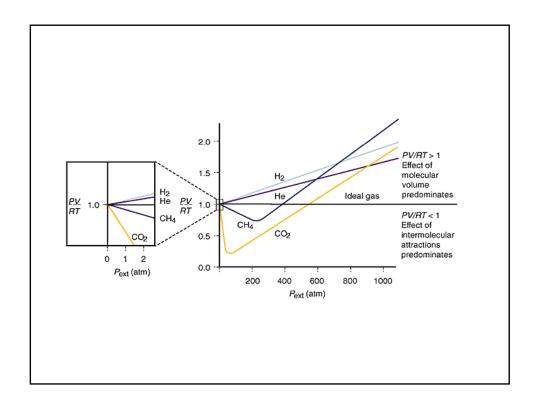


Fig. 1.14 The variation of the compression factor, Z, with pressure for several gases at 0°C. A perfect gas has Z=1 at all pressures. Notice that, although the curves approach 1 as $p \to 0$, they do so with different slopes.



Virial equation of state

The observation of a Z factor different from unity can be used to construct an empirical or observation based equation of state, by supposing that the ideal gas equation of state is only the first term of a more complex expression which can be expressed in terms of a mathematical power series. This is called the Virial equation of state.

$$Z = \frac{PV_m}{RT} = 1 + \frac{B}{V_m} + \frac{C}{V_m^2} + \dots = 1 + B'P + C'P^2$$

$$V_m \to \infty$$

$$P \to 0$$

p = 0: Close to ideal gas law, but not exact

p increases: B contributes, linear relation between Z and P

p higher: C and higher order terms contribute, deviation from linearity

Note that the virial coefficients B, C, B' and C' are obtained by fitting the experimental Z vs P data to the virial equation of state. Their values depend on the identity of the gas and Reflect the presence of intermolecular forces and interactions.

When the pressure P is small the molar volume V_m will be very large and so the second and third terms in the virial series will be very small and to a good approximation the virial equation of state reduces to the ideal gas equation of state.

Virial: comes from that Latin word *vis*, *viris*, meaning force - the coefficients in the **virial equation** depend on the forces of interaction between molecules of the gas

Boyle Temperature

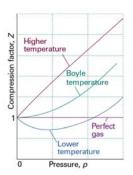


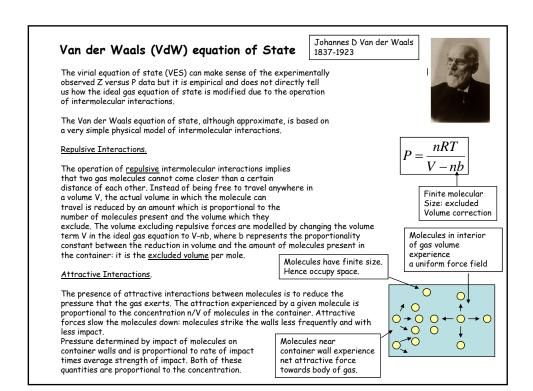
Fig. 1.16 The compression factor, Z, approaches 1 at low pressures, but does so with different slopes. For a perfect gas, the slope is zero, but real gases may have either positive or negative slopes, and the slope may vary with temperature. At the Boyle temperature, the slope is zero and the gas behaves perfectly over a wider range of conditions than at other temperatures.

In a perfect gas dZ/dP = 0 (since Z = 1). In a real gas the result is different.

$$\frac{dZ}{dP} = B' + 2PC' + \dots \cong B' \text{ as } P \to 0$$

$$\frac{dZ}{d(1/V_m)} \cong B \text{ as } V_m \to \infty$$

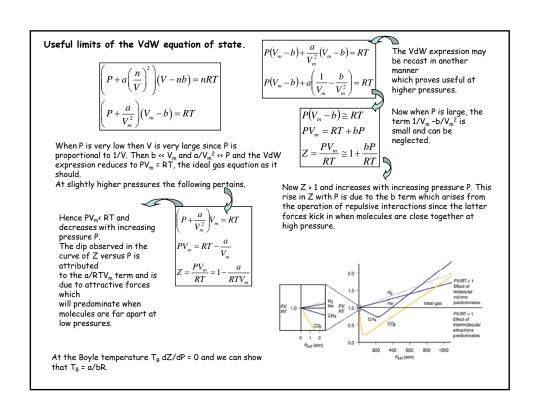
At low T the initial dZ/dP < 0, B is negative. At high T the initial dZ/dP > 0 and B is positive. The temperature at which the initial slope is zero is Termed the Boyle Temperature T_B where B = 0. Here the real gas behaves as an ideal gas.



Reduction in pressure proportional to $(n/V)^2 = a(n/V)^2$ where a denotes a constant of proportionality which takes account of attractive interactions. Hence this correction factor should be added to the pressure P to make up for this deficit, and the Pressure term in the ideal gas equation of state is changed from P to P + $a(n/V)^2$.

Measured pressure $P = \frac{nRT}{V - nb} - a\left(\frac{n}{V}\right)^2$ Correction factor to account for Intermolecular attractions

We equation of state VdW equation of state VdW equation of state $P + a\left(\frac{n}{V}\right)^2 \left(V - nb\right) = nRT$ $V_m = \frac{V}{n}$



a/(atm dm ⁴ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) a/(atm dm ⁴ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) Ar 1.337 3.20 H ₂ S 4.84 4.34 C ₂ H ₄ 4.552 5.82 He 0.0341 2.38 C ₂ H ₈ 5.507 6.51 Kr 5.125 1.06	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Air	Air	Air	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Air	Air	Air	Air	Air	Air	Air -167.3 -13.5 3.4 19.0 Ar -187.0 -21.7 -4.2 11.9 CH ₄ -55.6 -21.2 8.1 CO ₂ -142 -72.2 -12.4 H ₂ -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr -62.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 N ₃ -160.0 -10.5 6.2 21.7 N ₆ -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 The matrix of the subset relate to the expansion in eqn 1.22 of Section 1.30x convert to eqn 1.21 using $B^* = BBT$. For Ar at 273 K, $C = 1200$ cm ⁵ mod ⁴ .	Air -167.3 -13.5 3.4 19.0 Ar -187.0 -21.7 -4.2 11.9 CH ₄ -53.6 -21.2 8.1 CO ₂ -142 -72.2 -12.4 H ₂ -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr -62.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 N ₃ -160.0 -10.5 6.2 21.7 N ₆ -6.9 -28.7 1.7 N ₇ -160.0 -10.5 6.2 21.7 N ₈ -160.0 -10.5 6.2 21.7 N ₉ -160.0 -10.5 6.2 21.7 N ₉ -160.0 -10.5 6.2 11.3 Data AIP, II. The values relate to the expansion in eqn 1.22 of Section 1.38; convert to eqn 1.21 using $B^{\sigma} = BBT$. For Ar at 273 K, $C = 1200 \text{cm}^{\sigma} \text{mol}^{-1}$.	Air	Air -167.3 -13.5 3.4 19.0 Ar -187.0 -21.7 -4.2 11.9 CH ₄ -55.6 -21.2 8.1 CO ₂ -142 -72.2 -12.4 H ₂ -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr -62.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -153.7 -81.7 -19.6 Data: AIP, IL The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $df = BRT$. For Ar at 277 K, $C = 1200$ cm ⁶ mol ⁻¹ .	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Air -167.3 -13.5 3.4 19.0 Ar -187.0 -21.7 -4.2 11.9 C14 -53.6 -21.2 8.1 CO ₂ -142 -72.2 -12.4 H ₂ -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr -62.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -2.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 -19.6 Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.30; convert to eqn 1.21 using $B^* = BRT$. For Ar at 273 K, $C = 1200$ cm 6 mod 4 .	Air -167.3 -13.5 3.4 19.0 Ar -187.0 -21.7 -4.2 11.9 CH ₄ -53.6 -21.2 8.1 CO ₂ -142 -72.2 -12.4 H ₂ -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr -62.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -2.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 -19.6 Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B' = BBT$. For Ar at 273 K, $C = 1200$ cm ⁶ mod ⁻¹ .	Air -167.3 -13.5 3.4 19.0 Ar -187.0 -21.7 -4.2 11.9 C14, -53.6 -21.2 8.1 CO ₂ -142 -72.2 -12.4 H ₂ -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr -62.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -153.7 -81.7 -19.6 Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.30c convert to eqn 1.21 using $8^n = 8RT$. For N_1 at 273 K, $C = 1200$ cm ⁴ mol ⁻¹ .	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Air -167.3 -13.5 3.4 19.0 At -167.0 -21.7 -4.2 11.9 CH ₄ -53.6 -21.2 8.1 CO ₂ -142 -72.2 -12.4 H ₂ -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr -6.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 -19.6 Data: AIP, IL The values relate to the expansion in oqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B' = BBT'$. For A at 273 K, $C = 1200$ cm ⁶ mod ⁻¹ .	Air -167.3 -13.5 3.4 19.0 At -167.0 -21.7 -4.2 11.9 CH ₄ -53.6 -21.2 8.1 CO ₂ -142 -72.2 -12.4 H ₂ -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr -6.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 -19.6 Data: AIP, IL The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B' = BBT$. For A at 275 K, $C = 1200$ cm ⁶ mod ⁺¹ .	Air -167.3 -13.5 3.4 19.0 Ar -167.0 -21.7 -4.2 11.9 CH ₄ -55.6 -21.2 8.1 CO ₂ -142 -72.2 -12.4 H ₂ -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr -62.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₃ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 -19.6 Date AIP, IL. The valuer relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $g^* = g(RT)$. For Ar at 273 K, $C = 1200$ cm ⁶ mof ⁴ .	Air -167.3 -13.5 3.4 19.0 Ar -187.0 -21.7 -4.2 11.9 CH ₄ -53.6 -21.2 8.1 CO ₂ -142 -72.2 -12.4 H ₂ -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr -62.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 -19.6 Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.30; convert to eqn 1.21 using $B' = BBTT$. For Ar at 273 K, $C = 1200$ cm ⁶ mod ² .	Air -167.3 -13.5 3.4 19.0 At -187.0 -21.7 -4.2 11.9 CH ₄ -53.6 -21.2 8.1 CO ₂ -142 -72.2 -12.4 H ₂ -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr -62.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 -19.6 Date AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B' = BIRT$. For Ar at 273 K, $C = 1200$ cm ⁴ mod ⁴ .	Air -167.3 -13.5 3.4 19.0 Ar -187.0 -21.7 -4.2 11.9 CH ₄ -55.6 -21.2 8.1 CO ₂ -142 -72.2 -12.4 H ₂ -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr -62.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 -19.6 Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B' = BBTT$. For Ar at 273 K, $C = 1200$ cm ⁴ mod ⁴ .
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CH ₄	CH4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	CH4	CH4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	CH4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	CH4	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccc} CH_4 & -53.6 & -21.2 & 8.1 \\ CO_2 & -142 & -72.2 & -12.4 \\ H_2 & -2.0 & 13.7 & 15.6 \\ He & 11.4 & 12.0 & 11.3 & 10.4 \\ Kr & -62.9 & -28.7 & 1.7 \\ N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \\ \hline \\ Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using. \\ B'' = BBT. \\ For Ar at 273 K, C = 1200 cm^4 mol^{-3}. \\ \hline $	$ \begin{array}{c ccccc} CH_4 & -53.6 & -21.2 & 8.1 \\ CO_2 & -142 & -72.2 & -12.4 \\ H_2 & -2.0 & 13.7 & 15.6 \\ He & 11.4 & 12.0 & 11.3 & 10.4 \\ Kr & -62.9 & -28.7 & 1.7 \\ N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -133.7 & -81.7 & -19.6 \\ \hline \\ Data: AID, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using. \\ BF = BRT. \\ For Ar at 273 K, C = 1200 cm^6 mol^4. \\ \hline \\ \textbf{Fable 1.6 } \ \ \text{van} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	$ \begin{array}{c ccccc} CH_4 & -53.6 & -21.2 & 8.1 \\ CO_2 & -142 & -72.2 & -12.4 \\ H_2 & -2.0 & 13.7 & 15.6 \\ He & 11.4 & 12.9 & 11.3 & 10.4 \\ Kr & -62.9 & -28.7 & 1.7 \\ N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \\ \hline \\ Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B' = BRT. For Ar at 273 K, C = 1200 \mathrm{cm}^4 mol2+.$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccc} CH_4 & -53.6 & -21.2 & 8.1 \\ CO_2 & -142 & -72.2 & -12.4 \\ H_2 & -2.0 & 13.7 & 15.6 \\ He & 11.4 & 12.0 & 11.3 & 10.4 \\ Kr & -62.9 & -28.7 & 1.7 \\ N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -133.7 & -81.7 & -19.6 \\ \hline \\ Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B^* = BRT. For Ar at 273 K, C = 1200 \mathrm{cm}^4 mol4.$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	CO2	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccc} CO_2 & -142 & -72.2 & -12.4 \\ H_2 & -2.0 & 13.7 & 15.6 \\ He & 11.4 & 12.0 & 11.3 & 10.4 \\ Kr & -6.29 & -28.7 & 1.7 \\ N_3 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \\ \hline Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B=BBT. For Ar at 273 K, C=1200\mathrm{cm}^4\mathrm{mol}^{-1},$	CO2	$ \begin{array}{c ccccc} CO_1 & -142 & -72.2 & -12.4 \\ H_2 & -2.0 & 13.7 & 15.6 \\ He & 11.4 & 12.0 & 11.3 & 10.4 \\ Kr & -6.29 & -28.7 & 1.7 \\ N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \\ \hline Data: AIP, IL. The values relate to the expansion in oqn 1.22 of Section 1.3b; convert to oqn 1.21 using B^* = BBT. For Ar at 273 K, C = 1200 \mathrm{cm}^6 \mathrm{mol}^{2.4}.$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	CO2 -142 -72.2 -12.4 H2 -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Ke -62.9 -28.7 1.7 Ny -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O2 -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Data AIP, IL. The values relate to the expansion in opn 1.22 of Section 1.3b; convert to opn 1.21 using 18° -8 DCT. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ .	CO2	CO2 -142 -72.2 -12.4 H2 -2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr -62.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Dear AIP, IL: The values relate to the expansion in opn 1.22 of Section 1.3b; convert to opn 1.21 using 18' = BRT. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ .	CO2 - 142 - 72.2 - 12.4 H2 - 2.0 13.7 15.6 He 11.4 12.0 11.3 10.4 Kr6.9 - 28.7 1.7 N3 - 160.0 - 10.5 6.2 21.7 Ne6.0 10.4 12.3 13.8 O2 - 197.5 - 22.0 - 3.7 12.9 Xe - 197.5 - 22.0 - 3.7 12.9 Data AIP, IL. The values relate to the expansion in opn 1.22 of Section 1.3b; convert to opn 1.21 using 18' = BRT. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ .
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Table 1.6 van der Waals coefficients a/(atm dm ⁶ mol ⁻²) b/(10 ⁻² dm ⁵ mol ⁻¹) a/(atm dm ⁶ mol ⁻²) b/(10 ⁻² dm ⁵ mol ⁻¹) Ar 1.337 3.20 H ₂ S 4.484 4.55 C ₂ H ₄ 4.532 5.82 He 0.0341 2.38 C ₂ H ₄ 4.532 5.82 He 0.0341 2.38 C ₂ H ₄ 5.507 6.51 Kr 0.5125 1.06	He	He	He	He	He	He 11.4 12.0 11.3 10.4 Kr 1-6.19 - 11.3 10.4 Kr 1-6.19 - 12.6 7 1.7 N2 - 160.0 - 10.5 6.2 21.7 N2 - 160.0 - 10.5 6.2 21.7 N2 - 160.0 10.4 12.3 13.8 O2 - 197.5 - 22.0 - 3.7 12.9 N2 - 153.7 - 11.7 - 19.6 O2 - 153.7 - 11.7 - 19.6 O2 - 153.7 - 11.7 - 19.6 O2 - 153.7 O2 - 153.7 O3 - 15.7 O3 - 15.7 O3	He 11.4 12.0 11.3 10.4 Kr 1-6.19 - 11.3 10.4 Kr 1-6.19 - 12.6 7 1.7 N2 - 160.0 - 10.5 6.2 21.7 N2 - 160.0 - 10.5 6.2 21.7 N2 - 160.0 10.4 12.3 13.8 O2 - 197.5 - 22.0 - 3.7 12.9 N2 - 153.7 - 11.7 - 19.6 O2 - 153.7 - 11.7 - 19.6 O2 - 153.7 - 11.7 - 19.6 O2 - 153.7 O2 - 153.7 O3 - 15.7 O3 - 15.7 O3	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	He	He	He 11.4 12.0 11.3 10.4 Kr -6.9 -28.7 1.7 N ₁ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Data: AIP, IL: The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values relate to the expansion in opt 1.22 of Section 1.3b; convert to eqn 1.21 using the AIP, III. The values rel	He 11.4 12.0 11.3 10.4 Kr -62.9 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -153.7 -81.7 -19.6 Date: AIP, IL. The values relate to the expansion in opn 1.22 of Section 1.3b; convert to opn 1.21 using d' = BIRT. For Ar at 273 K, C = 1200 cm ⁴ mol ⁻¹ . all(atm dm ⁴ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) al/(atm dm ⁴ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) r 1.337 3.20 H ₁ S 4.464 4.34	He 11.4 12.0 11.3 10.4 Kr -62.9 -28.7 1.7 N ₁ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Date: APE, IL. The values relate to the expansion in our 1.22 of Section 1.3b; convert to our 1.21 using 8° = 807. For Ar at 273 K, C=1200 cm ⁶ mol ⁻¹ . Table 1.6 van der Waals coefficients ###################################	He 11.4 12.0 11.3 10.4 Kr $-62.9 -28.7 1.7$ N2 $-160.0 -10.5 6.2 21.7$ Ne $-60.0 10.4 12.3 13.8$ O2 $-197.5 -22.0 -3.7 12.9$ Xe $-197.5 -22.0 -3.7 12.9$ Data: AIP, IL: The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B = BBT$. For $Ax \neq 275$ K, $C = 1200$ cm 6 mol $^{-1}$.	He 11.4 12.0 11.3 10.4 Kr $-61.9 - 12.87$ 1.7 Nz $-160.0 - 10.5$ 6.2 21.7 Ne $-60.0 - 10.5$ 6.2 21.7 Ne $-60.0 - 10.4$ 12.3 13.8 Oz -197.5 $-22.0 - 3.7$ 12.9 Xe -197.5 $-22.0 - 3.7$ 12.9 The Late AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.38; convert to eqn 1.21 using $B^* = BBT$. For Ar at 273 K, $C = 1200 \mathrm{cm}^4 \mathrm{mol}^{-1}$.	He 11.4 12.0 11.3 10.4 Kr -62.9 -78.7 1.7 N2 -160.0 -10.5 6.2 21.7 N2 -160.0 10.4 12.3 13.8 O2 -79.7 12.9 N2 -197.5 -22.0 -3.7 12.9 N2 -197.5 -22.0 -3.7 12.9 N2 -197.5 N2 -193.3 -81.7 -19.6 Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using 8° = BRT. For Ar at 273 K, C = 1200 cm ³ mol ²⁺ .	He 11.4 12.0 11.3 10.4 Kr $-6.29 - 28.7 1.7$ 1.7 N ₂ $-160.0 - 10.5 6.2 21.7$ N ₂ $-160.0 - 10.5 6.2 21.7$ Ne $-6.0 10.4 12.3 13.8$ O ₂ $-197.5 - 22.0 - 3.7 12.9$ Xe $-197.5 - 22.0 - 3.7 12.9$ Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B^* = BBT$. For Ar at 273 K, $C = 1200 \text{cm}^4$ mol ⁴ .		He	He	He	He	He 11.4 12.0 11.3 10.4 Kr -6.29 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Xe -153.7 -81.7 -19.6 Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B^* = BIRT$. For Ar at 27.3 K, $C = 1200 \text{cm}^4 \text{mol}^{-1}$.	He 11.4 12.0 11.3 10.4 Kr -62.9 -18.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using 8° = 8RT. For Ar at 273 K, C = 1200 cm ⁵ mol ²⁺ .	He 11.4 12.0 11.3 10.4 Kr -62.9 -18.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 The material of the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using 8° = BRT. For Ar at 273 K, C = 1200 cm ⁴ mol ⁴ .	He 11.4 12.0 11.3 10.4 Kr -6.29 -28.7 1.7 N ₂ -160.0 -10.5 6.2 21.7 N ₃ -160.0 -10.5 6.2 21.7 Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Xe -153.7 -81.7 -19.6 Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B^* - BBT$. For Ar at 273 K, $C = 1200 \mathrm{cm}^4 \mathrm{mol}^4$.
	Kr			Kr	Kr		Kr	Kr	Kr	Kr	Kr	Kr	Kr	Kr													
	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		N2		$ N_2 - 160.0 - 10.5 - 6.2 - 21.7 \\ Ne - 6.0 - 10.4 - 12.3 - 13.8 \\ O_2 - 197.522.03.7 - 12.9 \\ Xe - 197.5153.781.719.6 \\ \hline Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using. \\ B' = BIRT. \\ For Ar at 273 K, C = 1200 cm^6 mol^{-1}. $		$ \begin{aligned} N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \\ \\ \hline Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B^{\prime\prime}=BBT$. For Ar at 273 K, $C=1200\mathrm{cm^{\prime\prime}}$ molt $^{\prime\prime}$.	$ \begin{aligned} N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \end{aligned} $ $ \begin{aligned} Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.30; convert to eqn 1.21 using 8° = 8RT. \\ For Ar at 273 K, C = 1200 cm^6 mol^4. \end{aligned} $	$ \begin{aligned} N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \end{aligned} $ Data: AIP, IL: The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B' = BRT$. For Ar at 273 K, $C = 1200 \mathrm{cm}^6 \mathrm{mol}^{-1}$.		$ \begin{aligned} N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \end{aligned} $ $ Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B^* = BRT.$ For A at 273 K, $C = 1200 cm^6$ mol$^-1$. $	$ \begin{aligned} N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_1 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \\ \hline Date AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B' = BBTT. For A at 273 K, C = 1200 \mathrm{cm}^4 \mathrm{mol}^{-1}. & & & & & & & & & & & & & & & & & & $	$ \begin{aligned} N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \\ \hline Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B' = BBT. For A at 273 K, C = 1200 \mathrm{cm}^6 \mathrm{mol}^{-1}. & & & & & & & & & & & & & & & & & & $	$ \begin{aligned} N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \\ \hline Date AIP, IL The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B' = BBT. For A at 273 K, C = 1200 \mathrm{cm}^4 \mathrm{mol}^{-1}. & & & & & & & & & & & & & & & & & & $	$ \begin{aligned} N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \\ \hline \\ Date AIP, [L. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B^* = BIKT. For Ar at 273 K, C = 1200 \mathrm{cm}^4 mof ^4.$	$ \begin{aligned} N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \end{aligned} $ Data: AIP, IL-The values relate to the expansion in eqn 1.22 of Section 1.30; convert to eqn 1.21 using $B^* = BRT$. For Ar at 273 K, $C = 1200 \mathrm{cm}^6$ mod 2 .	$ \begin{aligned} N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \\ \hline \\ Date: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B' = BRT. For Ar at 273 K, C = 1200 \mathrm{cm}^4 mod ^4. \end{aligned} $	$ \begin{aligned} N_2 & -160.0 & -10.5 & 6.2 & 21.7 \\ Ne & -6.0 & 10.4 & 12.3 & 13.8 \\ O_2 & -197.5 & -22.0 & -3.7 & 12.9 \\ Xe & -153.7 & -81.7 & -19.6 \\ \hline \\ Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B' = BRT. For Ar at 273 K, C = 1200 \mathrm{cm}^4 mod ^4.$
Ne	Ne	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Ne	Ne							Ne	Ne -6.0 10.4 12.3 13.8 0.2 -197.5 -22.0 -3.7 12.9 -2.0 -3.7 -3	Ne	Ne -6.0 10.4 12.3 13.8 $O_2 - 197.5$ -22.0 -3.7 12.9 $O_3 - 197.5$ -22.0 -3.7 12.9 $O_4 - 197.5$ $O_5 - 197.5$ $O_7 - 199.6$ Data: AIP, IL: The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using. $B' = BBT$. For Ar at 273 K, $C = 1200$ cm 6 mol $^{-1}$. Abilo 1.6 van der Waals coefficients $a'/a \text{tart dm}^6 \text{ mol}^{-2}$ $b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$ $a'/(a \text{tart dm}^6 \text{ mol}^{-2})$ $b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$	Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Section 1.38. Convert to eqn 1.21 using $B^{*}=BBT$. For Ar at 273 K, $C=1200$ cm ⁶ mol ⁻¹ .	Ne	Ne		Ne -6.0 10.4 12.3 13.8 0.7 1.7 12.6 13.8 0.7 12.9 2.6 2.7 12.9 2.7 12.0 13.7 12.9 2.7 12.0 13.8 2.7 12.0 13.8 2.7 12.0 13.8 2.7 12.0 2.	Ne -6.0 10.4 12.3 13.8 0.7 -197.5 -22.0 -3.7 12.9	Ne -6.0 10.4 12.3 13.8 0.2 -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Xe -197.5 -19.6 Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B^* = BRT$. For A r at 273 K, $C = 1200 \text{cm}^4 \text{mol}^{-1}$.	Ne -6.0 10.4 12.3 13.8 0.2 -197.5 -22.0 -3.7 12.9 Ye -197.5 -22.0 -3.7 -19.6 Ye -153.7 -81.7 -19.6 Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using. We also relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using. For Ar at 273 K, $C = 1200 \mathrm{cm}^4 \mathrm{mol}^{-1}$.	Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Ye -153.7 -61.7 -19.6 Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B^* = B/RT$. For A r at 273 K, $C = 1200$ cm 4 mod $^{-4}$.	Ne -6.0 10.4 12.3 13.8 O ₁ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Ye -197.5 -2.0 15.3.7 -81.7 -19.6 Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B* = BRT. For Ar at 273 K, C = 1200 cm* mol**.	Ne -6.0 10.4 12.3 13.8 O ₂ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Ye -153.7 -81.7 -19.6 Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B^* = BRT$. For Ar at 273 K, $C = 1200 \mathrm{cm}^4 \mathrm{mol}^{-4}$.	Ne -6.0 10.4 12.3 13.8 O ₁ -197.5 -22.0 -3.7 12.9 Xe -197.5 -22.0 -3.7 12.9 Te -197.5 -19.5 -19.5 -19.6 Data AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B^* = BRT$. For Ar at 273 K, $C = 1200 \mathrm{cm}^4 \mathrm{mod}^{-4}$.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	O₂ −197.5 −22.0 −3.7 12.9 Xe −193.7 −81.7 −19.6 Data: AIP, II. The values relate to the expansion in ogn 1.22 of Section 1.30; convert to egn 1.21 using ## ### ### ### ### ### ### ### ### ##	O ₂	O ₂	O ₂	O2	O ₂ -197.5 -22.0 -3.7 12.9 Xe -193.5 -22.0 -3.7 12.9 Xe -153.7 -81.7 -19.6 Data, AIP, II. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using # = BRFT. For Ar at 273 K, C = 1200 cm ⁴ mol ⁻¹ . **Table 1.6 van der Waals coefficients **a/(stat dm ⁴ mol ⁻²)	O2	O2	O2	$\frac{O_2}{Xe} = -197.5 \qquad -22.0 \qquad -3.7 \qquad 12.9 \\ Xe = -153.7 \qquad -81.7 \qquad -19.6 \\ Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B = BRIT. For Ar at 273 K, C = 1200 \text{ cm}^4 \text{ mol}^{-1}, B = \frac{1}{4} A \text{ for the mol}^{-1} A for the mol$	$ O_2 = -197.5 = -22.0 = -3.7 = 12.9 \\ Xe = -153.7 = -81.7 = -19.6 \\ \hline Data: AIP, JL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B' = BBT. For Ar at 273 K, C = 1200 cm^6 mof^{-1}.$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \frac{O_2}{Xc} = -197.5 \qquad -22.0 \qquad -3.7 \qquad 12.9 \\ Xc \qquad -153.7 \qquad -81.7 \qquad -19.6 \\ \hline Data, AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B^* = BRT. For Ar at 273 K, C = 1200 \mathrm{cm}^4 \mathrm{mol}^{-1}. \frac{1}{4} = \frac{1}{4} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	O2 -197.5 -22.0 -3.7 12.9 Xe -153.7 -81.7 -19.6 Date: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using 18° = 18(27) K, C = 1200 cm ⁶ mol ⁻¹ . Table 1.6 van der Waals coefficients	$ O_1 = -197.5 \qquad -22.0 \qquad -3.7 \qquad 12.9 $ Xe $ -153.7 \qquad -81.7 \qquad -19.6 $ Date: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B' = BRT$. For Ar at 273 K, $C = 1200 \mathrm{cm}^6 \mathrm{mol}^{-1}$.	O ₂ -197.5 -22.0 -3.7 12.9 Xe -153.7 -81.7 -19.6 Date: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using 16° = RET. To Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ . Table 1.6 van der Waals coefficients	O ₁ -197.5 -22.0 -3.7 12.9 Xe -153.7 -81.7 -19.6 Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using 16° = R(ET, 10° +
					Xe	Xe	Xe	Xe	Xe	Xe	Xe	Xe		Xe	$\frac{Xe}{Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $d' = BRT.$ for $A'' at 275 $K, $C' = 1200 cm^6 mol^{-1}$.}$ $\frac{ablo 1.6 \text{ van der Waals coefficients}}{a'/atm dm^6 mol^{-2}} \frac{b/(10^{-2} dm^3 mol^{-1})}{a'/(atm dm^6 mol^{-2})} \frac{b/(10^{-2} dm^3 mol^{-1})}{b'/(10^{-2} dm^3 mol^{-1})}$	Xe —153.7 —81.7 —19.6 Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B = BBT. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ .	Xe —153.7 —81.7 —19.6 Data: AIP, IL-The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using 8° = 8077. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ . Fable 1.6 van der Waals coefficients	Xe —153.7 —81.7 —19.6 Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.30; convert to eqn 1.21 using 8° = 80°T. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ . Table 1.6 van der Waals coefficients				$ \frac{Xe}{Data: AIP, JL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B' = BBT. $BT.$$ For $Ax at 275 K, $C = 1200 cm^6 mol^4$. $	$ \frac{Xe}{Data: AIP, JL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B' = BBT. $BT.$$ For $Ax at 275 K, $C = 1200 cm^6 mol^4$. $	Xe —153.7 —81.7 —19.6 Data: AIP, JL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B* a BET. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ . Table 1.6 van der Waals coefficients	Xe —153.7 —81.7 —19.6 Data: AIP, IL-The values relate to the expansion in eqn 1.22 of Section 1.30; convert to eqn 1.21 using # = BETT. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ . Fable 1.6 van der Waals coefficients	Xe —153.7 —81.7 —19.6 Date AIP, JL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using # = BET. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ . Fable 1.6 van der Waals coefficients	Xe —153.7 —81.7 —19.6 Data: AIP, IL-The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using # = BETT. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ . Fable 1.6 van der Waals coefficients
Data: AIP, IL: The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using b' = B/RT.	Data: AIP, IL. The values relate to the expansion in oqn 1.22 of Section 1.3b; convert to eqn 1.21 using B' = BET. For Ar at 273 K, C = 1200 cm ⁶ mot ⁻¹ .	Dotts: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.30c, convert to eqn 1.21 using b' = RFLT. For Ar at 273 K, C = 1200 cm ⁴ mol ⁻¹ . Table 1.6 van der Waals coefficients a/(stm dm ⁴ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) a/(stm dm ⁴ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) Ar 1.337 3.20 H₂S 4.484 4.34 2.38 C₂H₂ 4.532 5.82 H∉ 0.0341 2.38 C₂H₂ 5.507 6.51 Kr 5.125 1.06 C₂H₂ 18.57 11.93 N₂ 1.352 3.87 3.87	Dotts: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.30c, convert to eqn 1.21 using b' = RFLT. For Ar at 273 K, C = 1200 cm ⁴ mol ⁻¹ . Table 1.6 van der Waals coefficients a/(stm dm ⁴ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) a/(stm dm ⁴ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) Ar 1.337 3.20 H₂S 4.484 4.34 2.38 C₂H₂ 4.532 5.82 H∉ 0.0341 2.38 C₂H₂ 5.507 6.51 Kr 5.125 1.06 C₂H₂ 18.57 11.93 N₂ 1.352 3.87 3.87	Data: AIP, IL. The values relate to the expansion in oqn 1.22 of Section 1.3b; convert to eqn 1.21 using th' = RET.	Data: AIP, IL: The values relate to the expansion in oqn 1.22 of Section 1.3b; convert to eqn 1.21 using: #f = RET; For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ . Fable 1.6 van der Waals coefficients a/(atm dm ⁶ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) a/(atm dm ⁶ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) Vr	Data: AIP; IL: The values relate to the expansion in oqn 1.22 of Section 1.3b; convert to eqn 1.21 using: $B^* = BBT$; For Ar at 273 K, $C = 1200$ cm 4 mol $^{-1}$. able 1.6 van der Waals coefficients al (stm dm 4 mol $^{-2}$) $b/(10^{-2}$ dm 3 mol $^{-1}$) al (stm dm 4 mol $^{-2}$) $b/(10^{-2}$ dm 3 mol $^{-1}$) r 1.337 3.20 H ₂ S 4.484 4.34 $g/4$ 4.552 5.82 He 0.0341 2.38 $g/4$ 5.507 6.51 Kr 5.125 1.06	Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.30s, convert to eqn 1.21 using. $B^a = BBT$. For Ar at 273 K, $C = 1200 \text{ cm}^6 \text{ mol}^{-1}$. able 1.6 van der Waals coefficients $a/(\text{atm dm}^6 \text{ mol}^{-2})$ $b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$ $a/(\text{atm dm}^6 \text{ mol}^{-2})$ $b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$ r 1.337 3.20 H ₂ S 4.484 4.34 $a^2/4$ 4.552 5.82 He 0.0541 2.28	Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.30s, convert to eqn 1.21 using. $B^a = BBT$. For Ar at 273 K, $C = 1200 \text{ cm}^6 \text{ mol}^{-1}$. able 1.6 van der Waals coefficients $a/(\text{atm dm}^6 \text{ mol}^{-2})$ $b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$ $a/(\text{atm dm}^6 \text{ mol}^{-2})$ $b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$ r 1.337 3.20 H ₂ S 4.484 4.34 $a^2/4$ 4.552 5.82 He 0.0541 2.28	Data: AIP, IL The values relate to the expansion in eqn 1.22 of Section 1.30s, convert to eqn 1.21 using B' = B(BT.' For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ .	Data: AIP, IL The values relate to the expansion in eqn 1.22 of Section 1.30c convert to eqn 1.21 using B' = B BT For Ar at 275 K, C = 1200 cm ⁶ mol ⁻¹ . For Ar at 275 K, C = 1200 cm ⁶	Data: AIP, IL The values relate to the expansion in eqn 1.22 of Section 1.30s, convert to eqn 1.21 using B' = B BT. For As at 275 K, C = 1200 cm ⁶ mol ⁻¹ .	Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using f' = R/RT. For Art at 273 K, C = 1200 cm ⁴ mol ⁻¹ .	Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using B'= B/RT, Each of a 273 K, C = 1200 cm ⁶ mok ⁻¹ .	Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using	Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B = BRT$. For Ar at 273 K, $C = 1200 \text{cm}^4 \text{mol}^{-1}$. suble 1.6 van der Waals coefficients $a/(\text{atm dm}^4 \text{mol}^{-2}) \qquad b/(10^{-2} \text{dm}^3 \text{mol}^{-1}) \qquad a/(\text{atm dm}^4 \text{mol}^{-2}) \qquad b/(10^{-2} \text{dm}^3 \text{mol}^{-1})$	Data: AIP, JL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B' = ROPT$. For Ar at 273 K, $C = 1200$ cm ⁶ mol ⁻¹ .	Data: AIP, IL. The values relate to the expansion in oqn 1.22 of Section 1.3b; convert to oqn 1.21 using $B^* = BRT$. For Ar at 273 K, $C = 1200 \text{ cm}^4 \text{ mol}^{-1}$. Fable 1.6 van der Waals coefficients	Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using th' = IRET. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ . Table 1.6 van der Waals coefficients	Date: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B^* = BRT$. For Ar at 277 K, $C = 1200$ cm 4 mol $^{-1}$. Table 1.6 van der Waals coefficients $a/(atm dm^4 mol^{-2}) \qquad b/(10^{-2} dm^3 mol^{-1}) \qquad a/(atm dm^4 mol^{-2}) \qquad b/(10^{-2} dm^3 mol^{-1})$	Data: AIP; IL: The values relate to the expansion in eqn 1.22 of Section 1.30; convert to eqn 1.21 using $B^* = BRT$. For Ar at 273 K, $C = 1200 \text{ cm}^4 \text{ mol}^{-1}$. Table 1.6 van der Waals coefficients $a/(\text{atm dm}^4 \text{ mol}^{-2}) \qquad b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1}) \qquad a/(\text{atm dm}^4 \text{ mol}^{-2}) \qquad b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$	Data: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.30; convert to eqn 1.21 using $B^* = RRT$. For Ar at 273 K, $C = 1200 \text{ cm}^4 \text{ mol}^{-1}$. Fable 1.6 van der Waals coefficients $a/(\text{atm dm}^4 \text{ mol}^{-2}) \qquad b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1}) \qquad a/(\text{atm dm}^4 \text{ mol}^{-2}) \qquad b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$	Data: AIP, JL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B^* = B(BT)$. For Ar at 273 K, $C = 1200 \text{ cm}^4 \text{ mol}^{-1}$. Fable 1.6 van der Waals coefficients $a/(\text{atm dm}^4 \text{ mol}^{-2}) \qquad b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1}) \qquad a/(\text{atm dm}^4 \text{ mol}^{-2}) \qquad b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$	Data: AIP, JL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using $B^* = B(BT)$. For Ar at 273 K, $C = 1200 \text{ cm}^4 \text{ mol}^{-1}$. Fable 1.6 van der Waals coefficients $a/(\text{atm dm}^4 \text{ mol}^{-2}) \qquad b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1}) \qquad a/(\text{atm dm}^4 \text{ mol}^{-2}) \qquad b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$	Date: AIP, IL. The values relate to the expansion in eqn 1.22 of Section 1.3b; convert to eqn 1.21 using \$8^* = B/RT\$. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ . Cable 1.6 van der Waals coefficients	Data: AIP, IL. The values relate to the expansion in oqn 1.22 of Section 1.3b; convert to oqn 1.21 using #* = RRT. For Ar at 273 K, C = 1200 cm ⁶ mol ² . Fable 1.6 van der Waals coefficients	Date: AIP, IL. The values relate to the expansion in oan 1.22 of Section 1.3b; convert to oan 1.21 using #* = RFT. For Ar at 273 K, G = 1200 cm ⁶ mol ⁻¹ . Fable 1.6 van der Waals coefficients	Data: AIP, IL. The values relate to the expansion in oqn 1.22 of Section 1.3b; convert to oqn 1.21 using #* = RRT. For Ar at 273 K, C = 1200 cm ⁶ mol ² . Fable 1.6 van der Waals coefficients
## ## ## ## ## ## ## ## ## ## ## ## ##	### #### #### ########################	## ## ## ## ## ## ## ## ## ## ## ## ##	## ## ## ## ## ## ## ## ## ## ## ## ##	Fable 1.6 van der Waals coefficients	### ### ### ### ### ### ### ### ### ##	## ### ### ### ### ### ### ### ### ###	## BURT. For Ar at 273 K, C = 1200 cm ⁴ mol ⁻¹ . ## able 1.6 van der Waals coefficients ## a/(atm dm ⁶ mol ⁻²)	## BURT. For Ar at 273 K, C = 1200 cm ⁴ mol ⁻¹ . ## able 1.6 van der Waals coefficients ## a/(atm dm ⁶ mol ⁻²)	## BIRT. For Ar at 273 K, C = 1200 cm ⁴ mol ⁻¹ . ### Albert 1.6 van der Waals coefficients #### al/(atm dm ⁴ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) #/(atm dm ⁴ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) ###################################	## BRT. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ . Fable 1.6 van der Waals coefficients ### a// (atm dm ⁶ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) #// (atm dm ⁶ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) ar 1.337 3.20 H ₂ S 4.484 4.34 ar 4.552 5.82 He 0.0541 2.38	## BIRT. For Ar at 273 K, C = 1200 cm ⁴ mol ⁻¹ . Fable 1.6 van der Waals coefficients a/(atm dm ⁴ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) a/(atm dm ⁶ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) ar 1.337 3.20 H ₂ S 4.484 4.34 -2.14 -2.15 -2.14 -2.15 -2.15 -2.25 -2.25 -2.26 -2.2	### ### ### ### ### ### ### ### ### ##	## BERT. For Ar at 273 K, C = 1200 cm ⁶ mol ⁻¹ . ## able 1.6 van der Waals coefficients ## al/satm dm ⁶ mol ⁻²) ## b/(10 ⁻² dm ³ mol ⁻¹) ## al/satm dm ⁶ mol ⁻²) ## b/(10 ⁻² dm ³ mol ⁻¹) ## 1.337 ## 3.20 ## 5 ## 4.464 ## 4.34	## BIRT. For Art at 273 K, C = 1200 cm ⁴ mol ⁻¹ . **Cable 1.6 van der Waals coefficients ## a/(atm dm ⁴ mol ⁻²)	$ablo \ 1.6 \ van \ der \ Waals \ coefficients$ $a / (atm \ dm^{6} \ mol^{-2}) \qquad b / (10^{-2} \ dm^{3} \ mol^{-1}) \qquad a / (atm \ dm^{6} \ mol^{-2}) \qquad b / (10^{-2} \ dm^{3} \ mol^{-1})$	$B'=BBT$. For Ar at 273 K, $C=1200~{\rm cm}^6$ mol ⁻¹ .	$B^* = BRT$. For Ar at 273 K, $C = 1200$ cm 4 mod 4 .	B' = BRT. For Ar at 273 K, $C = 1200$ cm h mol $^{+}$. Table 1.6 van der Waals coefficients	$a/(atm dm^4 mol^{-2}) b/(10^{-2} dm^3 mol^{-1})$ Table 1.6 van der Waals coefficients $a/(atm dm^4 mol^{-2}) b/(10^{-2} dm^3 mol^{-1}) a/(atm dm^4 mol^{-2}) b/(10^{-2} dm^3 mol^{-1})$	$B^{\prime\prime} = BRT.$ For Ar at 273 K, $C = 1200 \text{cm}^4 \text{mol}^{-1}$. Fable 1.6 van der Waals coefficients $a/(a \text{tm dm}^4 \text{mol}^{-2}) \qquad b/(10^{-2} \text{dm}^3 \text{mol}^{-1}) \qquad a/(a \text{tm dm}^4 \text{mol}^{-2}) \qquad b/(10^{-2} \text{dm}^3 \text{mol}^{-1})$	Fable 1.6 van der Waals coefficients $a/(atm dm^4 mol^{-2}) b/(10^{-2} dm^3 mol^{-1}) \qquad a/(atm dm^4 mol^{-2}) b/(10^{-2} dm^3 mol^{-1})$	Fable 1.6 van der Waals coefficients $a/(a t m dm^{4} mol^{-2}) \qquad b/(10^{-2} dm^{3} mol^{-1}) \qquad a/(a t m dm^{4} mol^{-2}) \qquad b/(10^{-2} dm^{3} mol^{-1})$	Fable 1.6 van der Waals coefficients $a/(a t m dm^{4} mol^{-2}) \qquad b/(10^{-2} dm^{3} mol^{-1}) \qquad a/(a t m dm^{4} mol^{-2}) \qquad b/(10^{-2} dm^{3} mol^{-1})$	B* BERT. For Ar at 273 K, C = 1200 cm ⁴ mod ⁻¹ . Table 1.6 van der Waals coefficients	$B^* = BRT$. For Ar at 273 K, $C = 1200 \mathrm{cm}^4$ mol 4 .	B^* = BRT. For Ar at 273 K, $C = 1200$ cm 4 mod 4 .	$B^* = BRT$. For Ar at 273 K, $C = 1200 \text{cm}^4 \text{mod}^{-4}$. Fable 1.6 van der Waals coefficients
Ar 1,337 3,20 H ₂ S 4,484 4,34 C ₂ H ₄ 4,552 5,82 He 0,0541 2,38 C ₂ H ₈ 5,507 6,51 Kr 5,125 1,06	Ar 1.337 3.20 H,S 4.484 4.34 C,H4 4.552 5.82 He 0.0541 2.38 C,H ₈ 5.507 6.51 Kr 5.125 1.06	Ar 1.337 3.20 H.S 4.484 4.34 C.H, 4.552 5.82 Hr 0.0341 2.38 C.H, 5.307 6.51 Kr 5.125 1.06 C.H, 18.57 11.93 N ₂ 1.352 3.87	Ar 1.337 3.20 H.S 4.484 4.34 C.H, 4.552 5.82 Hr 0.0341 2.38 C.H, 5.307 6.51 Kr 5.125 1.06 C.H, 18.57 11.93 N ₂ 1.352 3.87	Ar 1.337 3.20 H,S 4.484 4.34 2,H ₄ 4.552 5.82 He 0.0341 2.38 2,H ₈ 5.507 6.51 Kr 5.125 1.06	kr 1.337 3.20 H,S 4.484 4.34 2H ₄ 4.552 5.82 He 0.0341 2.38 2H ₈ 5.507 6.51 Kr 5.125 1.06	r 1,337 3,20 H,S 4,484 4,34 ₄ H ₄ 4,552 5,82 He 0,0341 2,38 ₅ H ₆ 5,507 6,51 Kr 5,125 1,06	r 1,337 3,20 H,S 4,484 4,34 ₂ H ₄ 4,552 5,82 He 0,0541 2,38	r 1,337 3,20 H,S 4,484 4,34 ₂ H ₄ 4,552 5,82 He 0,0541 2,38	r 1,337 3,20 H ₂ S 4,484 4,34 ₂ H ₄ 4,552 5,82 He 0,0041 2,38	ur 1,337 3,20 H,S 4,484 4,34 _G H ₄ 4,552 5,82 He 0,0341 2,38	ır 1,337 3,20 H ₂ S 4,484 4,34 ₁₂ H ₄ 4,552 5,82 He 0,0341 2,38	ur 1,337 3,20 H ₂ S 4,484 4,34	r 1.337 3.20 H ₂ S 4.484 4.34	ur 1.337 3.20 H ₂ S 4.484 4.34		a/(atm dm ⁶ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) a/(atm dm ⁶ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹)	$a/(a \text{tm dm}^6 \text{ mol}^{-2})$ $b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$ $a/(a \text{tm dm}^6 \text{ mol}^{-2})$ $b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$	$a/(a \text{tm dm}^6 \text{ mol}^{-2})$ $b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$ $a/(a \text{tm dm}^6 \text{ mol}^{-2})$ $b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$						a/(atm dm ⁶ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) a/(atm dm ⁶ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹)	a/(atm dm ⁶ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) a/(atm dm ⁶ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹)	a/(stm dm ⁶ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹) a/(stm dm ⁶ mol ⁻²) b/(10 ⁻² dm ³ mol ⁻¹)	
C_2H_4 4.552 5.82 He 0.0341 2.38 C_2H_6 5.507 6.51 Kr 5.125 1.06	C_2H_4 4.552 5.82 He 0.0341 2.38 C_2H_6 5.507 6.51 Kr 5.125 1.06	C ₂ H ₁ 4.552 5.82 Hr 0.0341 2.38 C ₂ H ₈ 5.307 6.51 Kr 5.125 1.06 C ₂ H ₈ 18.57 11.93 N ₂ 1.352 3.87	C ₂ H ₁ 4.552 5.82 Hr 0.0341 2.38 C ₂ H ₈ 5.307 6.51 Kr 5.125 1.06 C ₂ H ₈ 18.57 11.93 N ₂ 1.352 3.87	C ₂ H ₆ 4.552 5.82 He 0.0341 2.38 C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	_H ₄ 4.552 5.82 He 0.0341 2.38 _H ₅ 5.507 6.51 Kr 5.125 1.06	H ₄ 4.552 5.82 He 0.0341 2.38 H ₅ 5.507 6.51 Kr 5.125 1.06	₄ H ₄ 4.552 5.82 He 0.0341 2.38	₄ H ₄ 4.552 5.82 He 0.0341 2.38	₄ H ₄ 4.552 5.82 He 0.0341 2.38	L ₁ H ₄ 4.552 5.82 He 0.0341 2.38	L ₂ H ₄ 4.552 5.82 He 0.0341 2.38				1,337 3,20 H.S 4,484 4,34							1122				arrangement to the sum and the	$a/(a \text{tm dm}^6 \text{ mol}^{-2})$ $b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$ $a/(a \text{tm dm}^6 \text{ mol}^{-2})$ $b/(10^{-2} \text{ dm}^3 \text{ mol}^{-1})$
C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87	T ₂ H ₈ 5.507 6.51 Kr 5.125 1.06	² H ₈ 5.507 6.51 Kr 5.125 1.06	H ₆ 5.507 6.51 Kr 5.125 1.06						L ₄ 4.552 5.82 He 0.0341 2.38	H 4552 582 He 0.0341 2.38												Ar 1,337 3,20 H,S 4,484 4,34		
		C ₆ H ₆ 18.57 11.93 N ₂ 1.352 3.87	C ₆ H ₆ 18.57 11.93 N ₂ 1.352 3.87				₂ H ₆ 5,507 6,51 Kr 5,125 1.06	.H. 5.507 6.51 Kr 5.125 1.06	.H. 5.507 6.51 Kr 5.125 1.06					2H ₄ 4.552 5.82 He 0.0341 2.38	H. 4.552 5.82 He 0.0341 2.38							TH 4552 5.82 He 0.000 3.34					
C ₄ H ₄ 18.57 11.93 N, 1.352 3.87	C ₆ H ₆ 18.57 11.93 N ₂ 1.352 3.87			C ₄ H ₆ 18.57 11.93 N ₂ 1.352 3.87	T.H. 18 57 11.03 N. 1.352 3.87						2H ₆ 5.507 6.51 Kr 5.125 1.06	LH. 5.507 6.51 Kr 5.125 1.06													C ₂ H ₄ 4.552 5.82 He 0.0341 2.38	C ₂ H ₄ 4.552 5.82 He 0.0341 2.38	C ₂ H ₄ 4.552 5.82 He 0.0341 2.38
							4H ₆ 18.57 11.93 N ₂ 1.352 3.87	H 16 57 11 03 N 1 157 5 87							H _a 5.507 6.51 Kr 5.125 1.06	H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₈ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	T ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	2H ₈ 5.507 6.51 Kr 5.125 1.06	² H ₈ 5.507 6.51 Kr 5.125 1.06	H ₆ 5.507 6.51 Kr 5.125 1.06	Cit H ₆ 4.352 5.82 He 0.0341 2.38 Cit H ₆ 5.507 6.51 Kr 5.125 1.06	_H4 4.552 5.82 He 0.0341 2.38 _H5 5.507 6.51 Kr 5.125 1.06	GH ₄ 4.552 5.82 He 0.0341 2.38 GH ₈ 5.507 6.51 Kr 5.125 1.06
	CH. 2.273 4.31 Ne 0.205 1.67	CH ₄ 2.273 4.31 Ne 0.205 1.67	CH ₄ 2.273 4.31 Ne 0.205 1.67	TH 2.273 4.31 No. 0.205 1.67								H ₆ 18.57 11.93 N ₂ 1.352 3.87	H ₆ 18.57 11.93 N ₂ 1.352 3.87	H ₆ 18.57 11.93 N ₂ 1.352 3.87	H ₈ 5.507 6.51 Kr 5.125 1.06 H ₆ 18.57 11.93 N ₂ 1.352 3.87	H ₆ 5.507 6.51 Kr 5.125 1.06 H ₆ 18.57 11.93 N ₂ 1.352 3.87	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N ₂ 1.352 3.87	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N ₂ 1.352 3.87	${}_{0}^{4}H_{6}$ 5.507 6.51 Kr 5.125 1.06 ${}_{0}^{4}H_{6}$ 18.57 11.93 N ₂ 1.352 3.87	$_{0}^{2}H_{h}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{h}$ 18.57 11.93 N ₂ 1.352 3.87	$_{0}^{2}H_{h}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{h}$ 18.57 11.93 N ₂ 1.352 3.87	H ₈ 5.507 6.51 Kr 5.125 1.06 ₆ H ₆ 18.57 11.93 N ₂ 1.352 5.87	_H, 4.552 5.82 He 0.0344 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87	_H, 4.552 5.82 He 0.034 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87	_H, 4.552 5.82 He 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.93 N ₂ 1.352 3.87
								H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	² ₆ H ₆ 18.57 11.93 N ₂ 1.352 3.87 2H ₄ 2.273 4.31 Ne 0.205 1.67	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	${}^{1}_{6}H_{6}$ 18.57 11.93 ${}^{1}N_{2}$ 1.352 3.67 ${}^{2}H_{4}$ 2.273 4.31 Ne 0.205 1.67	H_{k} 5.507 6.51 Kr 5.125 1.06 H_{t} 18.57 11.93 N_{2} 1.352 3.67 I_{4} 2.273 4.31 Ne 0.205 1.67	H_6 5.507 6.51 Kr 5.125 1.06 H_6 18.57 11.93 N ₂ 1.352 3.67 H_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N ₂ 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N ₂ 1.352 3.87 CH_4 2.273 4.31 Ne 0.205 1.67	C_0H_8 5.507 6.51 Kr 5.125 1.06 C_0H_8 18.57 11.93 N ₂ 1.352 3.87 CH_4 2.223 4.31 Ne 0.205 1.67	C_2H_8 5.507 6.51 Kr 5.125 1.06 C_9H_8 18.57 11.93 N ₂ 1.352 3.87 CH_4 2.273 4.31 Ne 0.205 1.67	$\Gamma_0^2H_6$ 5.507 6.51 Kr 5.125 1.06 $\Gamma_0^2H_6$ 18.57 11.93 N ₂ 1.352 3.87 $\Gamma_0^2H_6$ 2.273 4.31 Ne 0.205 1.67	$\frac{1}{6}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $\frac{1}{6}H_{8}$ 18.57 11.93 N ₂ 1.352 3.87 $\frac{1}{6}H_{8}$ 2.273 4.31 Ne 0.205 1.67	$_{\eta}^{2}H_{\eta}$ 5.507 6.51 Kr 5.125 1.06 $_{\eta}^{2}H_{\eta}$ 18.57 11.93 N ₂ 1.352 3.67 $_{\eta}^{2}H_{\eta}$ 2.273 4.31 Ne 0.205 1.67	$_{q}^{2}H_{h}$ 5.507 6.51 Kr 5.125 1.06 $_{q}^{4}H_{h}$ 18.57 11.93 N ₂ 1.352 3.87 $_{q}^{2}H_{d}$ 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$^{2}_{1}H_{4}$ 4.552 5.82 He 0.0341 2.38 $^{2}_{1}H_{5}$ 5.97 6.51 Kr 5.125 1.06 $^{2}_{2}H_{6}$ 18.57 11.93 N ₂ 1.352 3.87 $^{2}_{1}H_{4}$ 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
Cl ₂ 6.260 5.42 NH ₃ 4.169 3.71	Cl ₂ 6.260 5.42 NH ₃ 4.169 3.71			3 ₂ 6.260 5.42 NH ₃ 4.169 3.71	D ₂ 6.260 5.42 NH ₃ 4.169 3.71	l ₂ 6.260 5.42 NH, 4.169 3.71	l ₂ 6.260 5.42 NH, 4.169 3.71	H ₁ 2.273 4.31 Ne 0.205 1.67 I ₂ 6.260 5.42 NH, 4.169 3.71	H ₄ 2.273 4.31 Ne 0.205 1.67 1 ₂ 6.260 5.42 NH, 4.169 3.71	H ₄ 2.273 4.31 Ne 0.205 1.67 I ₂ 6.260 5.42 NH, 4.169 3.71	H ₄ 2.273 4.31 Ne 0.205 1.67 I ₂ 6.260 5.42 NH, 4.169 3.71	H ₆ 18.57 11.93 N ₂ 1.352 3.87 H ₄ 2.273 4.31 Ne 0.205 1.67 J ₂ 6.260 5.42 NH, 4.169 3.71	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	H ₆ 18.57 11.93 N ₂ 1.352 3.87 H ₆ 2.273 4.31 Ne 0.205 1.67 I ₂ 6.260 5.42 NH ₃ 4.169 3.71	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	H_6 5.507 6.51 Kr 5.125 1.06 H_6 18.57 11.93 N_2 1.352 3.87 H_4 2.273 4.31 Ne 0.205 1.67 h_2 6.260 5.42 h_3 h_4 4.169 3.71	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	C_2H_1 5.507 6.51 Kr 5.125 1.06 C_4H_4 18.57 11.93 N ₂ 1.352 5.87 CH_4 2.223 4.31 Ne 0.205 1.67 Cl_2 6.260 5.42 NH ₁ 4.169 3.71	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\mathbb{C}_{2}\mathbb{H}_{4}$ 5.507 6.51 Kr 5.125 1.06 $\mathbb{C}_{2}\mathbb{H}_{4}$ 18.57 11.93 N ₂ 1.352 3.87 $\mathbb{C}_{1}\mathbb{H}_{4}$ 2.273 4.31 Ne 0.205 1.67 \mathbb{C}_{2} 6.260 5.42 NH ₃ 4.169 3.71	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$^{2}_{1}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $^{2}_{2}H_{8}$ 18.57 11.93 N ₂ 1.352 3.87 $^{2}_{3}H_{4}$ 2.273 4.31 Ne 0.205 1.67 $^{2}_{3}$ 1.50 5.42 NH ₃ 4.169 3.71	$^{2}_{1}H_{6}$ 5.507 6.51 Kr 5.125 1.06 $^{2}_{1}H_{6}$ 18.57 11.93 N ₂ 1.352 3.87 $^{2}_{2}H_{6}$ 2.273 4.31 Ne 0.205 1.67 $^{2}_{3}$ 6.260 5.42 NH ₃ 4.169 3.71	$^{2}_{1}H_{0}$ 5.507 6.51 Kr 5.125 1.06 $^{1}_{2}H_{0}$ 18.57 11.93 N ₂ 1.352 3.87 $^{1}_{4}$ 2.273 4.31 Ne 0.205 1.67 $^{1}_{2}$ 6.260 5.42 NH ₃ 4.169 3.71	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
CO 1.453 3.95 O ₂ 1.364 3.19	CD ₂ 6.260 5.42 NH ₃ 4.169 3.71 CO 1.453 3.95 O ₂ 1.364 3.19	CO 1.453 3.95 O ₂ 1.364 3.19	CO 1.453 3.95 O ₂ 1.364 3.19	D2 6.260 5.42 NH, 4.169 3.71 CO 1.453 3.95 O2 1.364 3.19	31 6.260 5.42 NH, 4.169 3.71 CO 1.453 3.95 O2 1.364 3.19	l ₂ 6.260 5.42 NH, 4.169 3.71 O 1.453 3.95 O ₂ 1.364 3.19	l ₂ 6.260 5.42 NH, 4.169 3.71 O 1.453 3.95 O ₂ 1.364 3.19	H ₄ 2.273 4.31 Ne 0.205 1.67 I ₂ 6.260 5.42 NH, 4.169 3.71 O 1.453 3.95 O ₂ 1.364 3.19	H ₄ 2.273 4.31 Ne 0.205 1.67 l ₂ 6.260 5.42 NH, 4.169 3.71 O 1.483 3.98 O ₂ 1.364 3.19	H ₄ 2.273 4.31 Ne 0.205 1.67 l ₂ 6.260 5.42 NH, 4.169 3.71 00 1.483 3.98 O ₂ 1.364 3.19	H ₄ 2.273 4.31 Ne 0.205 1.67 l ₂ 6.260 5.42 NH, 4.169 3.71 00 1.483 3.98 O ₂ 1.364 3.19	$^{\circ}_{n}H_{n}$ 18.57 11.93 N ₂ 1.352 3.87 H_{4} 2.273 4.31 Ne 0.205 1.67 J_{2} 6.260 5.42 NH, 4.169 3.71 2.0 1.453 3.95 O ₂ 1.364 3.19	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$^{2}_{6}H_{6}$ 18.57 11.93 N ₂ 1.352 3.87 H_{4} 2.273 4.31 Ne 0.205 1.67 J_{2} 6.260 5.42 NH, 4.169 3.71 J_{2} 1.453 3.95 O ₂ 1.364 3.19	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	H_6 5.307 6.51 Kr 5.125 1.06 H_6 18.57 11.93 N_2 1.352 3.87 H_6 2.273 4.31 Ne 0.205 1.67 h_7 6.260 5.42 h_7 h_7 4.169 3.71 h_7 0 1.483 3.95 h_7 1.364 3.19	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$^{-}_{1}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $^{-}_{2}H_{8}$ 18.57 11.93 N ₂ 1.352 3.87 $^{-}_{2}H_{4}$ 2.273 4.31 Ne 0.205 1.67 $^{-}_{3}$ 6.260 5.42 NH ₃ 4.169 3.71 $^{-}_{3}$ 6.206 5.42 NH ₃ 4.169 3.71 $^{-}_{3}$ 6.20 3.98 O ₂ 1.364 3.19	$^{-}_{1}H_{u}$ 5.507 6.51 Kr 5.125 1.06 $^{-}_{2}H_{3}$ 18.57 11.93 N ₂ 1.352 3.87 $^{-}_{3}H_{4}$ 2.273 4.31 Ne 0.205 1.67 $^{-}_{3}$ 6.260 5.42 NH ₃ 4.169 3.71 CO 1.483 3.98 O ₂ 1.364 3.19	$^{1}_{6}H_{6}$ 5.507 6.51 Kr 5.125 1.06 $^{1}_{6}H_{6}$ 18.57 11.93 N ₂ 1.352 3.87 $^{1}_{4}H_{4}$ 2.273 4.31 Ne 0.205 1.67 $^{1}_{2}$ 6.260 5.42 NH ₃ 4.169 3.71 $^{1}_{3}$ 0.0 1.483 3.98 O ₂ 1.364 3.19	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
Cl ₂ 6.260 5.42 NH ₁ 4.169 3.71 CO 1.483 3.95 O ₂ 1.364 3.19 CO ₂ 3.610 4.29 SO ₂ 6.775 5.68	CD ₂ 6.260 5.42 NH, 4.169 3.71 CO 1.483 3.98 O ₂ 1.364 3.19 CO ₂ 3.610 4.29 SO ₂ 6.775 5.68	CO 1.453 3.95 O ₂ 1.364 3.19 CO ₂ 3.610 4.29 SO ₂ 6.775 5.68	CO 1.453 3.95 O ₂ 1.364 3.19 CO ₂ 3.610 4.29 SO ₂ 6.775 5.68	C1 6.260 5.42 NH, 4.169 3.71 C0 1.453 3.95 O2 1.364 3.19 CO2 3.610 4.29 SO2 6.775 5.68	Q1 6.260 5.42 NH, 4.169 3.71 CO 1.453 3.95 O2 1.364 3.19 CO2 3.610 4.29 SO2 6.775 5.68	I ₂ 6.260 5.42 NH, 4.169 3.71 O 1.453 3.95 O ₂ 1.364 3.19 O ₂ 3.610 4.29 SO ₂ 6.775 5.68	I ₂ 6.260 5.42 NH, 4.169 3.71 O 1.453 3.95 O ₂ 1.364 3.19 O ₂ 3.610 4.29 SO ₂ 6.775 5.68	H ₄ 2.273 4.31 Ne 0.208 1.67 h ₂ 6.260 5.42 NH, 4.169 3.71 O 1.453 3.99 O ₂ 1.364 3.19 O ₂ 3.610 4.29 SO ₂ 6.775 3.68	H ₄ 2.273 4.31 Ne 0.208 1.67 J ₂ 6.260 5.42 NH, 4.169 3.71 O 1.483 3.99 O ₁ 1.364 3.19 O ₂ 3.610 4.29 SO ₂ 6.775 5.68	H ₄ 2.273 4.31 Ne 0.208 1.67 J ₂ 6.260 5.42 NH, 4.169 3.71 DO 1.483 3.99 O ₂ 1.364 3.19 DO ₂ 3.610 4.29 SO ₂ 6.775 5.68	H ₄ 2.273 4.31 Ne 0.205 1.67 J ₂ 6.260 5.42 NH, 4.169 3.71 OO 1.483 3.99 O ₂ 1.364 3.19 OO ₂ 3.610 4.29 SO ₂ 6.775 5.68	$^{\circ}_{11}H_{0}$ 18.57 11.93 N ₂ 1.352 3.87 $^{\circ}_{14}H_{0}$ 2.273 4.31 Ne 0.205 1.67 $^{\circ}_{1}$ 6.260 5.42 NH ₁ 4.169 3.71 $^{\circ}_{1}$ 70 1.453 3.95 O ₂ 1.364 3.19 $^{\circ}_{1}$ 70 4.29 SO ₂ 6.775 5.68	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$^{1}_{9}H_{6}$ 18.57 11.93 N ₂ 1.352 3.67 $^{1}_{4}H_{4}$ 2.273 4.31 Ne 0.205 1.67 $^{1}_{2}$ 6.260 5.42 NH ₃ 4.169 3.71 $^{1}_{3}$ 70 1.453 3.95 O ₂ 1.364 3.19 $^{1}_{3}$ 70 ₂ 3.610 4.29 SO ₂ 6.775 5.68	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$^{2}_{1}H_{4}$ 5.507 6.51 Kr 5.125 1.06 $^{2}_{1}H_{3}$ 18.57 11.93 N ₂ 1.352 3.87 $^{2}_{1}H_{4}$ 2.273 4.31 Ne 0.205 1.67 J ₂ 6.260 5.42 NH ₂ 4.169 3.71 0.0 1.483 3.98 O ₂ 1.364 3.19 $^{2}_{1}$ 3.610 4.29 S ₂ 6.775 5.68	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	${}_{2}^{4}H_{4}$ 5.507 6.51 Kr 5.125 1.06 ${}_{4}^{4}H_{5}$ 16.57 11.93 N ₂ 1.352 3.67 ${}_{4}^{4}H_{4}$ 16.57 11.93 N ₂ 0.205 1.67 ${}_{4}^{2}$ 4.31 Ne 0.205 1.67 ${}_{4}^{2}$ 6.260 5.42 NH ₃ 4.169 3.71 0.0 1.483 3.98 O ₂ 1.364 3.19 0.0 ₂ 3.610 4.29 SO ₂ 6.775 5.68	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
Cl ₂ 6.260 5.42 NH, 4.169 3.71 CO 1.483 3.95 O ₂ 1.364 3.19 CO ₂ 3.610 4.29 SO ₂ 6.775 5.68 H ₂ 0.2420 2.65 Xe 4.137 5.16	Cl ₂ 6.260 5.42 NH ₁ 4.169 3.71 CO 1.483 3.95 O ₂ 1.364 3.19 Co ₂ 3.610 4.29 SO ₂ 6.775 5.68 H ₂ 0.2420 2.65 Xe 4.137 5.16	CO 1.483 3.95 O ₂ 1.364 3.19 CO ₂ 3.610 4.29 SO ₂ 6.775 5.68 H ₂ 0.2420 2.65 Xe 4.137 5.16	CO 1.483 3.95 O ₂ 1.364 3.19 CO ₂ 3.610 4.29 SO ₂ 6.775 5.68 H ₂ 0.2420 2.65 Xe 4.137 5.16	\Box_2 6.260 5.42 NH, 4.169 3.71 \Box 0 1.453 3.95 \Box_2 1.364 3.19 \Box 0, 3.610 4.29 SO ₂ 6.775 5.68 \Box 1, 0.2420 2.65 Xe 4.137 5.16	J ₂ 6.260 5.42 NH, 4.169 3.71 DO 1.453 3.95 O ₂ 1.364 3.19 Do 3.610 4.29 SO ₂ 6.775 5.88 I ₂ 0.2420 2.65 Xe 4.137 5.16	I ₂ 6,260 5,42 NH, 4,169 3,71 O 1,453 3,95 O ₂ 1,364 3,19 O ₂ 3,610 4,29 SO ₂ 6,755 5,68 ½ 0,2430 2,65 Xe 4,137 5,16	I ₂ 6,260 5,42 NH, 4,169 3,71 O 1,453 3,95 O ₂ 1,364 3,19 O ₂ 3,610 4,29 SO ₂ 6,755 5,68 ½ 0,2430 2,65 Xe 4,137 5,16	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	H_4 2.273 4.31 Ne 0.205 1.67 I_2 6.260 5.42 NH , 4.169 3.71 NO 1.483 3.98 O_2 1.364 3.19 O_2 3.610 4.29 SO 6.775 5.68 I_2 0.2420 2.65 Xe 4.137 5.16	H_4 2.273 4.31 Ne 0.205 1.67 J_2 6.260 5.42 NH $_3$ 4.169 3.71 J_3 0.0 1.483 3.98 J_2 1.364 3.19 J_3 3.610 4.29 J_4 3.0 6.75 5.68 J_2 0.2420 2.65 J_4 4.137 5.16	H_4 2.273 4.31 Ne 0.205 1.67 J_2 6.260 5.42 NH , 4.169 3.71 J_3 0.0 1.483 3.98 J_2 1.364 3.19 J_3 3.610 4.29 J_4 5.0 6.75 5.68 J_2 0.2420 2.65 J_4 4.137 5.16	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$_{1}^{1}$ H ₄ 18.57 11.99 N ₂ 1.352 3.87 $_{2}^{1}$ 4.31 Ne 0.205 1.67 $_{3}^{1}$ 6.260 5.42 NH ₃ 4.169 3.71 O 1.453 3.95 O ₂ 1.364 3.19 O ₂ 3.610 4.29 SO ₂ 6.775 5.68 $_{2}^{1}$ 0.2420 2.65 Xe 4.137 3.16	$^{1}_{4}$ H ₄ 18.57 11.93 N ₂ 1.352 3.87 $^{1}_{4}$ 2.273 4.11 Ne 0.205 1.67 $^{1}_{2}$ 6.260 5.42 NH ₃ 4.169 3.71 1 00 1.453 3.95 O ₂ 1.364 3.19 1 02 3.610 4.29 SO ₂ 6.775 5.68 1 1.2 5.16	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
							₄ H ₆ 18.57 11.93 N ₂ 1.352 3.87				2H ₈ 5.507 6.51 Kr 5.125 1.06	LH. 5.507 6.51 Kr 5.125 1.06		₂ H ₄ 4,352 5.82 He 0.0341 2.38											Ar 1.337 3.20 H ₂ S 4.484 4.34		artain am mor) artis am mor) artis am mor)
		AND 100 1.07	neg and 101 195 95400 1.07			H 2.273 4.31 No. 0.205 1.67	H 2 273 4 31 Ne 0 205 1 67					H ₆ 18.57 11.93 N ₂ 1.352 3.87	H ₆ 18.57 11.93 N ₂ 1.352 3.87	H ₆ 18.57 11.93 N ₂ 1.352 3.87	$H_{8} = 5.507 \qquad 6.51 \qquad Kr = 5.125 \qquad 1.06 \\ H_{6} = 18.57 \qquad 11.93 \qquad N_{2} = 1.352 \qquad 5.87$	H ₆ 5.507 6.51 Kr 5.125 1.06 H ₆ 18.57 11.93 N ₂ 1.352 3.87	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87	${}^{-}_{1}H_{6}$ 5.507 6.51 Kr 5.125 1.06 ${}^{-}_{10}H_{6}$ 18.57 11.93 ${}^{-}_{12}$ 1.352 3.87	$_{0}^{2}H_{h}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{h}$ 18.57 11.93 N_{2} 1.352 3.87	$_{0}^{2}H_{h}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{h}$ 18.57 11.93 N_{2} 1.352 3.87	$_{0}^{2}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{6}$ 18.57 11.93 N_{2} 1.352 3.87	_H, 4.552 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87	_H, 4.552 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87	_H, 4.552 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87
								H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	² ₆ H ₆ 18.57 11.93 N ₂ 1.352 3.87 2H ₄ 2.273 4.31 Ne 0.205 1.67	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	¹ ₄ H ₆ 18.57 11.93 N ₂ 1.352 3.87 H ₆ 2.273 4.31 Ne 0.205 1.67	$H_{8} = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ H_{9} = 18.57 \qquad 11.93 \qquad N_{2} \qquad 1.352 \qquad 3.87 \\ I_{4} = 2.273 \qquad 4.31 \qquad Ne \qquad 0.205 \qquad 1.67$	H_6 5.507 6.51 Kr 5.125 1.06 H_6 18.57 11.93 N ₂ 1.352 3.87 H_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.907 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87 CH_4 2.273 4.31 Ne 0.205 1.67	C_0H_8 5.507 6.51 Kr 5.125 1.06 C_0H_8 18.57 11.93 N ₂ 1.352 3.87 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	${}_{0}^{1}H_{6}$ 5.507 6.51 Kr 5.125 1.06 ${}_{0}^{1}H_{6}$ 18.57 11.93 N ₂ 1.352 3.67 ${}_{2}^{1}H_{4}$ 2.273 4.31 Ne 0.205 1.67	$_{\eta}^{2}H_{\eta}$ 5.507 6.51 Kr 5.125 1.06 $_{\eta}^{2}H_{\eta}$ 18.57 11.93 N ₂ 1.352 3.87 $_{\chi}^{2}H_{\eta}$ 2.273 4.31 Ne 0.205 1.67	$_{\eta}^{2}H_{\eta}$ 5.507 6.51 Kr 5.125 1.06 $_{\eta}^{2}H_{\eta}$ 18.57 11.93 N ₂ 1.352 3.87 $_{\chi}^{2}H_{\eta}$ 2.273 4.31 Ne 0.205 1.67	$_{q}^{2}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $_{q}^{4}H_{6}$ 18.57 11.93 N_{2} 1.352 3.87 H_{4} 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$^{2}_{4}H_{4}$ 4.552 5.82 He 0.0341 2.38 $^{2}_{4}H_{5}$ 5.97 6.51 Kr 5.125 1.06 $^{2}_{6}H_{6}$ 18.57 11.93 N ₂ 1.352 3.87 $^{2}_{4}H_{4}$ 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
								H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	² ₆ H ₆ 18.57 11.93 N ₂ 1.352 3.87 2H ₄ 2.273 4.31 Ne 0.205 1.67	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	¹ ₄ H ₆ 18.57 11.93 N ₂ 1.352 3.87 H ₆ 2.273 4.31 Ne 0.205 1.67	H_{8} 5.507 6.51 Kr 5.125 1.06 H_{9} 18.57 11.93 N_{2} 1.352 3.87 I_{4} 2.273 4.31 Ne 0.205 1.67	H_6 5.507 6.51 Kr 5.125 1.06 H_6 18.57 11.93 N ₂ 1.352 3.87 H_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N ₂ 1.352 3.87 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N ₂ 1.352 3.87 CH_4 2.273 4.31 Ne 0.205 1.67	$\Gamma_0^2H_6$ 5.507 6.51 Kr 5.125 1.06 $\Gamma_0^2H_6$ 18.57 11.93 N ₂ 1.352 3.67 $\Gamma_0^2H_4$ 2.273 4.31 Ne 0.205 1.67	$_{\eta}^{2}H_{\eta}$ 5.507 6.51 Kr 5.125 1.06 $_{\eta}^{2}H_{\eta}$ 18.57 11.93 N ₂ 1.352 3.67 $_{\chi}^{2}H_{\eta}$ 2.273 4.31 Ne 0.205 1.67	$_{\eta}^{2}H_{\eta}$ 5.507 6.51 Kr 5.125 1.06 $_{\eta}^{2}H_{\eta}$ 18.57 11.93 N ₂ 1.352 3.67 $_{\chi}^{2}H_{\eta}$ 2.273 4.31 Ne 0.205 1.67	$_{q}^{2}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $_{q}^{4}H_{6}$ 18.57 11.93 N_{2} 1.352 3.67 H_{4} 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$^{2}_{1}H_{4}$ 4.552 5.82 He 0.0341 2.38 $^{2}_{2}H_{5}$ 5.907 6.51 Kr 5.125 1.06 $^{2}_{3}H_{6}$ 18.57 11.93 N ₂ 1.352 3.87 $^{2}_{4}H_{4}$ 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
								H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	² ₆ H ₆ 18.57 11.93 N ₂ 1.352 3.87 2H ₄ 2.273 4.31 Ne 0.205 1.67	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	¹ ₄ H ₆ 18.57 11.93 N ₂ 1.352 3.87 H ₆ 2.273 4.31 Ne 0.205 1.67	$H_{8} = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ H_{9} = 18.57 \qquad 11.93 \qquad N_{2} \qquad 1.352 \qquad 3.87 \\ I_{4} = 2.273 \qquad 4.31 \qquad Ne \qquad 0.205 \qquad 1.67$	H_6 5.507 6.51 Kr 5.125 1.06 H_6 18.57 11.93 N ₂ 1.352 3.87 H_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.907 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87 CH_4 2.273 4.31 Ne 0.205 1.67	C_0H_8 5.507 6.51 Kr 5.125 1.06 C_0H_8 18.57 11.93 N_2 1.352 3.87 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	${}_{0}^{1}H_{6}$ 5.507 6.51 Kr 5.125 1.06 ${}_{0}^{1}H_{6}$ 18.57 11.93 N ₂ 1.352 3.67 ${}_{2}^{1}H_{4}$ 2.273 4.31 Ne 0.205 1.67	$_{\eta}^{2}H_{\eta}$ 5.507 6.51 Kr 5.125 1.06 $_{\eta}^{2}H_{\eta}$ 18.57 11.93 N ₂ 1.352 3.87 $_{\chi}^{2}H_{\eta}$ 2.273 4.31 Ne 0.205 1.67	$_{\eta}^{2}H_{\eta}$ 5.507 6.51 Kr 5.125 1.06 $_{\eta}^{2}H_{\eta}$ 18.57 11.93 N ₂ 1.352 3.87 $_{\chi}^{2}H_{\eta}$ 2.273 4.31 Ne 0.205 1.67	$_{q}^{2}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $_{q}^{4}H_{6}$ 18.57 11.93 N_{2} 1.352 3.87 H_{4} 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$^{2}_{4}H_{4}$ 4.552 5.82 He 0.0341 2.38 $^{2}_{4}H_{5}$ 5.97 6.51 Kr 5.125 1.06 $^{2}_{6}H_{6}$ 18.57 11.93 N ₂ 1.352 3.87 $^{2}_{4}H_{4}$ 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
At 14 0200 1.07	70 C TOUR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR C			110	31 ₄ 2.273 4.31 Ne 0.205 1.67	H ₆ 2.273 4.31 Ne 0.205 1.67	H ₄ 2,273 4.31 Ne 0,205 1.67					H ₆ 18.57 11.93 N ₂ 1.352 3.87	₄ H ₆ 18.57 11.93 N ₂ 1.352 3.87	H ₆ 18.57 11.93 N ₂ 1.352 3.87	$H_{8} = 5.507 \qquad 6.51 \qquad Kr = 5.125 \qquad 1.06 \\ H_{6} = 18.57 \qquad 11.93 \qquad N_{2} = 1.352 \qquad 3.87$	H ₆ 5.507 6.51 Kr 5.125 1.06 H ₆ 18.57 11.93 N ₂ 1.352 3.87	$\mathbb{C}_2 H_6 = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ \mathbb{C}_6 H_6 = 18.57 \qquad 11.93 \qquad N_2 \qquad 1.352 \qquad 3.87$	$\mathbb{C}_2 H_6 = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ \mathbb{C}_6 H_6 = 18.57 \qquad 11.93 \qquad N_2 \qquad 1.352 \qquad 3.87$	$\mathbb{C}_2 H_6 = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ \mathbb{C}_6 H_6 = 18.57 \qquad 11.93 \qquad N_2 \qquad 1.352 \qquad 3.87$	$\mathbb{C}_2 H_6 = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ \mathbb{C}_6 H_6 = 18.57 \qquad 11.93 \qquad N_2 \qquad 1.352 \qquad 3.87$	$\Gamma_0^2 H_6 = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ \Gamma_0 H_6 = 18.57 \qquad 11.93 \qquad N_2 \qquad 1.352 \qquad 3.87$	$_{0}^{2}H_{6}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{6}$ 18.57 11.93 N_{2} 1.352 3.87	$_{0}^{2}H_{6}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{6}$ 18.57 11.93 N_{2} 1.352 3.87	$_{0}^{2}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{9}$ 18.57 11.93 N_{2} 1.352 3.87	_H, 4.582 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87	_H, 4.552 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87	_H, 4.582 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87
								H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	² ₆ H ₆ 18.57 11.93 N ₂ 1.352 3.87 2H ₄ 2.273 4.31 Ne 0.205 1.67	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	¹ ₄ H ₆ 18.57 11.93 N ₂ 1.352 3.87 H ₆ 2.273 4.31 Ne 0.205 1.67	$H_{8} = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ H_{9} = 18.57 \qquad 11.93 \qquad N_{2} \qquad 1.352 \qquad 3.87 \\ I_{4} = 2.273 \qquad 4.31 \qquad Ne \qquad 0.205 \qquad 1.67$	H_6 5.507 6.51 Kr 5.125 1.06 H_6 18.57 11.93 N ₂ 1.352 3.87 H_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.907 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.907 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	${}_{0}^{1}H_{6}$ 5.507 6.51 Kr 5.125 1.06 ${}_{0}^{1}H_{6}$ 18.57 11.93 N ₂ 1.352 3.67 ${}_{2}^{1}H_{4}$ 2.273 4.31 Ne 0.205 1.67	$_{\eta}^{2}H_{\eta}$ 5.507 6.51 Kr 5.125 1.06 $_{\eta}^{2}H_{\eta}$ 18.57 11.93 N ₂ 1.352 3.87 $_{\chi}^{2}H_{\eta}$ 2.273 4.31 Ne 0.205 1.67	$_{\eta}^{2}H_{\eta}$ 5.507 6.51 Kr 5.125 1.06 $_{\eta}^{2}H_{\eta}$ 18.57 11.93 N ₂ 1.352 3.87 $_{\chi}^{2}H_{\eta}$ 2.273 4.31 Ne 0.205 1.67	$_{q}^{2}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $_{q}^{4}H_{6}$ 18.57 11.93 N_{2} 1.352 3.87 H_{4} 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$^{2}_{4}H_{4}$ 4.552 5.82 He 0.0341 2.38 $^{2}_{4}H_{5}$ 5.97 6.51 Kr 5.125 1.06 $^{2}_{6}H_{6}$ 18.57 11.93 N ₂ 1.352 3.87 $^{2}_{4}H_{4}$ 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
								H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	² ₆ H ₆ 18.57 11.93 N ₂ 1.352 3.87 2H ₄ 2.273 4.31 Ne 0.205 1.67	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	¹ ₄ H ₆ 18.57 11.93 N ₂ 1.352 3.87 H ₆ 2.273 4.31 Ne 0.205 1.67	$H_{8} = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ H_{9} = 18.57 \qquad 11.93 \qquad N_{2} \qquad 1.352 \qquad 3.87 \\ I_{4} = 2.273 \qquad 4.31 \qquad Ne \qquad 0.205 \qquad 1.67$	H_6 5.507 6.51 Kr 5.125 1.06 H_6 18.57 11.93 N ₂ 1.352 3.87 H_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	${}_{0}^{1}H_{6}$ 5.507 6.51 Kr 5.125 1.06 ${}_{0}^{1}H_{6}$ 18.57 11.93 N ₂ 1.352 3.67 ${}_{2}^{1}H_{4}$ 2.273 4.31 Ne 0.205 1.67	$_{\eta}^{2}H_{\eta}$ 5.507 6.51 Kr 5.125 1.06 $_{\eta}^{2}H_{\eta}$ 18.57 11.93 N ₂ 1.352 3.87 $_{\chi}^{2}H_{\eta}$ 2.273 4.31 Ne 0.205 1.67	$_{\eta}^{2}H_{\eta}$ 5.507 6.51 Kr 5.125 1.06 $_{\eta}^{2}H_{\eta}$ 18.57 11.93 N ₂ 1.352 3.87 $_{\chi}^{2}H_{\eta}$ 2.273 4.31 Ne 0.205 1.67	$_{q}^{2}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $_{q}^{4}H_{6}$ 18.57 11.93 N_{2} 1.352 3.87 H_{4} 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$^{2}_{4}H_{4}$ 4.552 5.82 He 0.0341 2.38 $^{2}_{4}H_{5}$ 5.97 6.51 Kr 5.125 1.06 $^{2}_{6}H_{6}$ 18.57 11.93 N ₂ 1.352 3.87 $^{2}_{4}H_{4}$ 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
								H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	H ₄ 2.273 4.31 Ne 0.205 1.67	² ₆ H ₆ 18.57 11.93 N ₂ 1.352 3.87 2H ₄ 2.273 4.31 Ne 0.205 1.67	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	¹ ₄ H ₆ 18.57 11.93 N ₂ 1.352 3.87 H ₆ 2.273 4.31 Ne 0.205 1.67	$H_{8} = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ H_{9} = 18.57 \qquad 11.93 \qquad N_{2} \qquad 1.352 \qquad 3.87 \\ I_{4} = 2.273 \qquad 4.31 \qquad Ne \qquad 0.205 \qquad 1.67$	H_6 5.507 6.51 Kr 5.125 1.06 H_6 18.57 11.93 N ₂ 1.352 3.87 H_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_5H_6 18.57 11.93 N_2 1.352 3.67 CH_4 2.273 4.31 Ne 0.205 1.67	${}_{0}^{1}H_{6}$ 5.507 6.51 Kr 5.125 1.06 ${}_{0}^{1}H_{6}$ 18.57 11.93 N ₂ 1.352 3.67 ${}_{2}^{1}H_{4}$ 2.273 4.31 Ne 0.205 1.67	$_{\eta}^{2}H_{\eta}$ 5.507 6.51 Kr 5.125 1.06 $_{\eta}^{2}H_{\eta}$ 18.57 11.93 N ₂ 1.352 3.87 $_{\chi}^{2}H_{\eta}$ 2.273 4.31 Ne 0.205 1.67	$_{\eta}^{2}H_{\eta}$ 5.507 6.51 Kr 5.125 1.06 $_{\eta}^{2}H_{\eta}$ 18.57 11.93 N ₂ 1.352 3.87 $_{\chi}^{2}H_{\eta}$ 2.273 4.31 Ne 0.205 1.67	$_{q}^{2}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $_{q}^{4}H_{6}$ 18.57 11.93 N_{2} 1.352 3.87 H_{4} 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$^{2}_{4}H_{4}$ 4.552 5.82 He 0.0341 2.38 $^{2}_{4}H_{5}$ 5.97 6.51 Kr 5.125 1.06 $^{2}_{6}H_{6}$ 18.57 11.93 N ₂ 1.352 3.87 $^{2}_{4}H_{4}$ 2.273 4.31 Ne 0.205 1.67	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
					3H ₄ 2,275 4.51 Ne 0,205 1.67	H _c 2.273 4.31 Ne 0.205 1.67	H _a 2,273 4.31 Ne 0.205 1.67					H ₆ 18.57 11.93 N ₂ 1.352 3.87	H ₆ 18.57 11.93 N ₂ 1.352 3.87	H ₆ 18.57 11.93 N ₂ 1.352 3.87	$H_{8} = 5.507 \qquad 6.51 \qquad Kr = 5.125 \qquad 1.06 \\ H_{6} = 18.57 \qquad 11.93 \qquad N_{2} = 1.352 \qquad 3.87$	H ₆ 5.507 6.51 Kr 5.125 1.06 H ₆ 18.57 11.93 N ₂ 1.352 3.87	$\mathbb{C}_2 H_6 = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ \mathbb{C}_6 H_6 = 18.57 \qquad 11.93 \qquad N_2 \qquad 1.352 \qquad 3.87$	$\mathbb{C}_2 H_6 = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ \mathbb{C}_6 H_6 = 18.57 \qquad 11.93 \qquad N_2 \qquad 1.352 \qquad 3.87$	$\mathbb{C}_2 H_6 = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ \mathbb{C}_6 H_6 = 18.57 \qquad 11.93 \qquad N_2 \qquad 1.352 \qquad 3.87$	$\mathbb{C}_2 H_6 = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ \mathbb{C}_6 H_6 = 18.57 \qquad 11.93 \qquad N_2 \qquad 1.352 \qquad 3.87$	$\Gamma_0^2 H_6 = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ \Gamma_0 H_6 = 18.57 \qquad 11.93 \qquad N_2 \qquad 1.352 \qquad 3.87$	$_{0}^{2}H_{6}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{6}$ 18.57 11.93 N_{2} 1.352 3.87	$_{0}^{2}H_{6}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{6}$ 18.57 11.93 N_{2} 1.352 3.87	$_{0}^{2}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{9}$ 18.57 11.93 N_{2} 1.352 3.87	_H, 4.582 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87	_H, 4.552 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87	_H, 4.582 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87
					34. 2.273 4.31 Ne 0.205 1.67	H. 2,273 4.31 Ne 0,205 1.67	H. 2,273 4,31 Ne 0,205 1,67					H ₆ 18.57 11.93 N ₂ 1.352 3.87	H ₆ 18.57 11.93 N ₂ 1.352 3.87	H ₆ 18.57 11.93 N ₂ 1.352 3.87	$H_{8} = 5.507 \qquad 6.51 \qquad Kr = 5.125 \qquad 1.06 \\ H_{6} = 18.57 \qquad 11.93 \qquad N_{2} = 1.352 \qquad 5.87$	H ₆ 5.507 6.51 Kr 5.125 1.06 H ₆ 18.57 11.93 N ₂ 1.352 3.87	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87	C_2H_8 5.507 6.51 Kr 5.125 1.06 C_4H_8 18.57 11.93 N_2 1.352 3.87	C_2H_8 5.507 6.51 Kr 5.125 1.06 C_6H_8 18.57 11.93 N_2 1.352 3.87	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87	$\Gamma_0^2 H_6 = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ \Gamma_0 H_6 = 18.57 \qquad 11.93 \qquad N_2 \qquad 1.352 \qquad 3.87$	$_{0}^{2}H_{h}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{h}$ 18.57 11.93 N_{2} 1.352 3.87	$_{0}^{2}H_{h}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{h}$ 18.57 11.93 N_{2} 1.352 3.87	$_{0}^{2}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{6}$ 18.57 11.93 N_{2} 1.352 3.87	_H, 4.552 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87	_H, 4.552 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87	_H, 4.552 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87
CH 2 273 4 31 No. 0 205 167	CH. 2,273 4,31 Ne 0,205 1,67	CH ₄ 2.273 4.31 Ne 0.205 1.67	CH ₄ 2.273 4.31 Ne 0.205 1.67	TH 2.273 4.31 No. 0.205 1.67								H ₆ 18.57 11.93 N ₂ 1.352 3.87	H ₆ 18.57 11.93 N ₂ 1.352 3.87	H ₆ 18.57 11.93 N ₂ 1.352 3.87	$H_{8} = 5.507 \qquad 6.51 \qquad Kr = 5.125 \qquad 1.06 \\ H_{6} = 18.57 \qquad 11.93 \qquad N_{2} = 1.352 \qquad 5.87$	H ₆ 5.507 6.51 Kr 5.125 1.06 H ₆ 18.57 11.93 N ₂ 1.352 3.87	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87	C_2H_8 5.507 6.51 Kr 5.125 1.06 C_4H_8 18.57 11.93 N_2 1.352 3.87	C_2H_8 5.507 6.51 Kr 5.125 1.06 C_4H_8 18.57 11.93 N_2 1.352 3.87	C_2H_6 5.507 6.51 Kr 5.125 1.06 C_6H_6 18.57 11.93 N_2 1.352 3.87	$\Gamma_0^2 H_6 = 5.507 \qquad 6.51 \qquad Kr \qquad 5.125 \qquad 1.06 \\ \Gamma_0 H_6 = 18.57 \qquad 11.93 \qquad N_2 \qquad 1.352 \qquad 3.87$	$_{0}^{2}H_{h}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{h}$ 18.57 11.93 N_{2} 1.352 3.87	$_{0}^{2}H_{h}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{h}$ 18.57 11.93 N_{2} 1.352 3.87	$_{0}^{2}H_{8}$ 5.507 6.51 Kr 5.125 1.06 $_{0}^{2}H_{6}$ 18.57 11.93 N_{2} 1.352 3.87	_H, 4.552 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87	_H, 4.552 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87	_H, 4.552 5.82 Hr 0.0341 2.38 _H, 5.507 6.51 Kr 5.125 1.06 _H, 18.57 11.99 N ₂ 1.352 3.87
	CH 2.379 (3) No. 0.305 1.67			THE DATE AND ADDRESS OF THE PARTY AND ADDRESS						LH. 18.57 11.93 N. 1.352 3.87	. H. 18.57 11.93 N. 1.352 3.87				H _a 5.507 6.51 Kr 5.125 1.06	H _s 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₈ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	T ₂ H ₈ 5.507 6.51 Kr 5.125 1.06	2H ₈ 5.507 6.51 Kr 5.125 1.06	2H ₈ 5.507 6.51 Kr 5.125 1.06	H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 4.552 5.82 He 0.0341 2.38 C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	_H4 4.552 5.82 He 0.0341 2.38 _H5 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 4.552 5.82 He 0.0341 2.38 C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06
							4H ₆ 18.57 11.93 N ₂ 1.352 3.87	H 16 57 11 03 N 1 357 3 67							H _a 5.507 6.51 Kr 5.125 1.06	H _s 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₈ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	T ₂ H ₈ 5.507 6.51 Kr 5.125 1.06	2H ₈ 5.507 6.51 Kr 5.125 1.06	2H ₈ 5.507 6.51 Kr 5.125 1.06	H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 4.552 5.82 He 0.0341 2.38 C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	_H4 4.552 5.82 He 0.0341 2.38 _H5 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 4.552 5.82 He 0.0341 2.38 C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06
						4H ₆ 18.57 11.93 N ₂ 1.352 3.87	₄ H ₆ 18.57 11.93 N ₂ 1.352 3.87	H 16.57 11.03 N 1.352 3.67				714 700	H ₆ 5,507 6,51 Kr 5,125 1.06	₂ H ₆ 5.507 6.51 Kr 5.125 1.06											C ₂ H ₄ 4.552 5.82 He 0.0341 2.38	C ₂ H ₄ 4.552 5.82 He 0.0341 2.38	C ₂ H ₄ 4.552 5.82 He 0.0341 2.38
	4.4						H 1857 1193 N. 1352 387						H. 5.507 6.51 Kr 5.125 1.06	.H. 5.507 6.51 Kr 5.125 1.06											C ₂ H ₄ 4.552 5.82 He 0.0341 2.38	C ₂ H ₄ 4.552 5.82 He 0.0341 2.38	C ₂ H ₄ 4.552 5.82 He 0.0341 2.38
						4H ₆ 18.57 11.93 N ₂ 1.352 3.87	₄ H ₆ 18.57 11.93 N ₂ 1.352 3.87	H 16.57 11.03 N 1.352 3.67				714 700	H ₆ 5,507 6,51 Kr 5,125 1.06	₂ H ₆ 5.507 6.51 Kr 5.125 1.06											C ₂ H ₄ 4.552 5.82 He 0.0341 2.38	C ₂ H ₄ 4.552 5.82 He 0.0341 2.38	C ₂ H ₄ 4.552 5.82 He 0.0341 2.38
						₆ H ₆ 18.57 11.93 N ₂ 1.352 3.87	₄ H ₆ 18.57 11.93 N ₂ 1.352 3.87	H 16.57 11.03 N 1.352 3.67				714 700	H ₆ 5,507 6,51 Kr 5,125 1.06	₂ H ₆ 5.507 6.51 Kr 5.125 1.06											C ₂ H ₄ 4.552 5.82 He 0.0341 2.38	C ₂ H ₄ 4.552 5.82 He 0.0341 2.38	C ₂ H ₄ 4.552 5.82 He 0.0341 2.38
						4H ₆ 18.57 11.93 N ₂ 1.352 3.87	₄ H ₆ 18.57 11.93 N ₂ 1.352 3.87	H 18 57 11 03 N 1 152 1 87				200 0000 0000	H _n 5.507 6.51 Kr 5.125 1.06	₂ H ₆ 5.507 6.51 Kr 5.125 1.06											C ₂ H ₄ 4.552 5.82 He 0.0341 2.38	C ₂ H ₄ 4.552 5.82 He 0.0341 2.38	C ₂ H ₄ 4.552 5.82 He 0.0341 2.38
					4.4	4H ₆ 18.57 11.93 N ₂ 1.352 3.87	4H ₆ 18.57 11.93 N ₂ 1.352 3.87	H 16 57 11 03 N 1 357 3 67							H _a 5.507 6.51 Kr 5.125 1.06	H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	T ₂ H ₈ 5.507 6.51 Kr 5.125 1.06	² H ₈ 5.507 6.51 Kr 5.125 1.06	² H ₈ 5.507 6.51 Kr 5.125 1.06	H ₆ 5.507 6.51 Kr 5.125 1.06	Cit H ₆ 4.352 5.82 He 0.0341 2.38 Cit H ₆ 5.507 6.51 Kr 5.125 1.06	_H4 4.552 5.82 He 0.0341 2.38 _H5 5.507 6.51 Kr 5.125 1.06	Cit H ₆ 4.352 5.82 He 0.0341 2.38 Cit H ₆ 5.507 6.51 Kr 5.125 1.06
							4R ₄ 18.57 11.95 N ₂ 1.552 3.87				1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				H _a 5.507 6.51 Kr 5.125 1.06	H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	T ₂ H ₈ 5.507 6.51 Kr 5.125 1.06	² H ₈ 5.507 6.51 Kr 5.125 1.06	² H ₈ 5.507 6.51 Kr 5.125 1.06	H ₆ 5.507 6.51 Kr 5.125 1.06	Cit H ₆ 4.352 5.82 He 0.0341 2.38 Cit H ₆ 5.507 6.51 Kr 5.125 1.06	_H4 4.552 5.82 He 0.0341 2.38 _H5 5.507 6.51 Kr 5.125 1.06	Cit H ₆ 4.352 5.82 He 0.0341 2.38 Cit H ₆ 5.507 6.51 Kr 5.125 1.06
											* U 16 57 11 03 N 1 153 1 47				H _a 5.507 6.51 Kr 5.125 1.06	H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	T ₂ H ₈ 5.507 6.51 Kr 5.125 1.06	² H ₈ 5.507 6.51 Kr 5.125 1.06	² H ₈ 5.507 6.51 Kr 5.125 1.06	H ₆ 5.507 6.51 Kr 5.125 1.06	Cit H ₆ 4.352 5.82 He 0.0341 2.38 Cit H ₆ 5.507 6.51 Kr 5.125 1.06	_H4 4.552 5.82 He 0.0341 2.38 _H5 5.507 6.51 Kr 5.125 1.06	Cit H ₆ 4.352 5.82 He 0.0341 2.38 Cit H ₆ 5.507 6.51 Kr 5.125 1.06
	THE AREA CO. LANS. NO. 140			THE ASSESSMENT ASSESSM						CH. 18 57 11 93 N. 1 352 3.87	. H. 18 57 11.93 N. 1.352 3.87				H _a 5.507 6.51 Kr 5.125 1.06	H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	C ₂ H ₆ 5.507 6.51 Kr 5.125 1.06	T ₂ H ₈ 5.507 6.51 Kr 5.125 1.06	² H ₈ 5.507 6.51 Kr 5.125 1.06	² H ₈ 5.507 6.51 Kr 5.125 1.06	H ₆ 5.507 6.51 Kr 5.125 1.06	Cit H ₆ 4.352 5.82 He 0.0341 2.38 Cit H ₆ 5.507 6.51 Kr 5.125 1.06	_H4 4.552 5.82 He 0.0341 2.38 _H5 5.507 6.51 Kr 5.125 1.06	Cit H ₆ 4.352 5.82 He 0.0341 2.38 Cit H ₆ 5.507 6.51 Kr 5.125 1.06

